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June 3, 1991

Mr. Manabu Tagamori
Department of Land and
Natural Resources
1151 Punchbowl Street
P.O. Box 373
Honolulu, Hawaii 96813

Dear Mr. Tagamori,

Please find enclosed copies of the summary reports of drilling operations for the Scientific Observation Hole Project, SOH-4 and SOH-1.

If you should have any questions, feel free to contact me at 522-5620.

Sincerely,

Harry J. Olson
Principal Investigator

bc: Dean Nakano

# SCIENTIFIC OBSERVATION HOLE #1
# KILAUEA EAST RIFT ZONE, HAWAII
# SUMMARY REPORT OF DRILLING OPERATIONS

Prepared By

John E. Deymonaz

May 1991

# Scientific Observation Hole #1

## PURPOSE AND SCOPE

The Scientific Observation Hole program ("SOH") was undertaken as both a scientific research project, and to aid in evaluating the geothermal potential of the Kilauea East Rift Zone on the island of Hawaii.

The SOH drilling is providing the first extensive core ever taken in Hawaii. Continuous core yields invaluable information to geologists and other earth scientists concerning the Kilauea East Rift Zone. This information can be utilized as a model to interpret the past geologic history of Hawaii and other islands in the Hawaiian Archipelago. It also offers a unique insight into the current and future volcanic and erosional activity along the rift zone. To geologists, the core is a tangible geologic record spanning a period of time which began when this part of Hawaii was still thousands of feet below sea level. The core provides detailed information of the islands evolution through periods of volcanic aggradation, erosion, sedimentation, mass wasting, intrusive activity and subsidence to its current state.

SOH drilling is also instrumental in evaluating the extent of a commercially viable geothermal resource along the East Rift Zone. Deep core, geophysical logs, temperature profiles and injection testing will assist both the state of Hawaii and private developers in understanding the nature of the resource and aid in establishing realistic resource development goals. The core in particular, offers an opportunity to study alteration, mineralization and fracturing in reservoir rock which is unavailable in conventional rotary drilled holes.

After completion and testing the SOH's will, as their name implies, serve as long term observation holes. They will provide stations to monitor the effects of geothermal production throughout the rift zone. Changes in temperature and pressure will be monitored and deep fluid samples may be collected.

SOH-1 was the second in a series of 4 planned Scientific Observation Holes to be drilled in the Kilauea East Rift Zone. The target depth for the SOH's is 4,000 to 6,500 feet. Actual completion depth of each hole depends on drilling conditions, temperature and a number of other factors which are evaluated on a continuing basis as the holes are drilled. The drilling program was designed to remain as flexable as possible to accommodate a variety of potential situations as they are encountered.

CONTRACTOR AND EQUIPMENT

Tonto Drilling Services Inc. of Salt Lake City, Utah is the drilling contractor chosen for the SOH program. Tonto has provided an experienced crew and the Universal 5000 rotary/core drilling rig to undertake this unique project. The Universal 5000 drilling rig is one of only two such units in existence and is uniquely suited for the requirements of the SOH project. It has been extensively modified for geothermal work and to meet stringent noise limitations mandated by the county of Hawaii.

The drilling rig is mounted on a 3-axle trailer and weighs approximately 94,600 pounds. A self-elevating jack-up system permits raising the rig and placing a 10.5 foot high substructure under the mast. The substructure carries the weight associated with drilling, serves as a working floor and permits the above ground installation of blow out prevention equipment ("BOPE").

Specifications for the Universal 5000 drill rig include:

a. Rotation head hoisting capacity of 100,000 pounds.

b. Main hoist capacity of 88,000 pounds (single line, 1-3/16 inch cable).

c. Rotation head pull down of 30,000 pounds.

d. Rotation head speed variable from 0 to 2,250 RPM.

e. Maximum rotation head output torque of 6,630 foot pounds.

f. Wireline winch with 18,000 feet of 3/8 inch wire rope and a full drum pull of up to 1,500 feet per minute.

g. Hydraulic system consisting of axial and radial piston pumps and motors designed as three independent open loop circuits.

h. 56 foot mast with a 40 foot rod pull and stacking capacity.

i. Hydraulically operated and self energizing casing and rod slips.

Depth rating of the Universal 5000 depends on the size of drill rods used, drilling conditions and other factors. In the case of NQ drill rods, which were used to complete SOH-1, the theoritical maximum depth is over 17,000 feet.

## DRILLING OPERATIONS

SOH-1 was spudded-in at 2 PM on May 31 and completed to a total depth of 5,526 feet G.L. (Ground Level) on December 21, 1990. A total of 205 working days was involved in drilling the hole. Following a break for Christmas, completion and testing involved an additional 15 days and the rig was released on January 13, 1991. A brief summary of drilling activities is presented in Table 1 and graphically illustrated in Figure 1.

### Surface Casing

SOH-1 was spudded-in with 101mm core (3.98" hole x 2.50" core) and drilled to 202 feet G.L. Total loss of drilling fluids occured at 25 feet and drilling continued without returns. The hole was then opened to 12-1/4 inches with a Hughes ATJ-33C tricone bit and near-bit welded blade stabalizer. Total loss of drilling fluids occured at 31 feet and drilling continued without returns to 202 feet.

9-5/8 inch K-55, 40 lb/ft buttress threaded and coupled casing was run open ended to 202 feet and set on bottom. The hole was dry to TD and the casing was cemented with 135 cubic feet of redimix concrete (5 sack mix w/ 1/2" minus aggregate). After 15 cubic feet of concrete was poured down the annulus, the casing was picked up off bottom several times to allow the cement to flow around the base of the casing and clean out any debris. The casing was then set back on bottom and the annulus filled with concrete to the surface.

Concrete volume was approximately 200% of theoretical, however, the annular space did not fill to surface. Cementing was completed with 3 top jobs using a total of 87 sacks of neat cement and 40 cubic feet of redimix.

Blow out prevention equipment (BOPE) was nippled up and tested to 600 psi. BOP equipment consisted of a 3M slip on wellhead with 2 inch flanged outlets, a 12 inch Type E double gate preventer with pipe and blind rams and 2 inch kill and flow lines attached to 2 inch 3M valves.

### Intermediate (Protection) Casing

From 11:00 AM on June 9 until 4:00 PM on June 14 (5.2 days) the contractor was put on standby awaiting a decision by the Hawaii County Planning Commission to permit the next phase of the drilling operation.

When drilling operations resumed, 101mm core drilling proceeded from 202 - 1,996 feet with partial return of drilling fluids. Core drilling began on June 14 and reached 1,996 feet on July 1, a total of 18 days.

After running a deviation survey (Table 8), the hole was opened to 8-1/2 inches from 202 - 1,996 feet using a 8-1/2 inch Hughes ATJ-33C tricone and near bit welded blade stabalizer.

Hole opening began on July 2 and reached 1,996 feet on July 25, a total of 24 days. The drill rods were tripped out of the hole and 7 inch L-80, 35 pound/foot buttress threaded and coupled casing was run. Float equipment consisted of a guide shoe and float collar at the top of the first joint (39.5 feet from bottom). When 1,800 feet of casing (63,000 pounds) had been run, the 1 inch cable on the main winch line snapped behind the socket and the casing string dropped into the hole. A fishing tool was fabricated and the lifting plug retrieved. The remaining 7 inch casing was stabbed into the dropped section and made up. After an 80,000 pound pull failed to pick up the casing, a 5-5/8 inch tricone was run in to the float collar to clean any debris and verify the casing integrity. On July 29 Halliburton Services was used to cement the 7 inch casing.

7 Inch Casing Cementing

Pump 40 bbls water, followed with 6 bbls super flush ahead of lead slurry.

| | |
|---|---|
| Lead slurry: | 49 bbl silica/spherelite cement (11 lb/gal, 88 sk cement, 4,400 lb spherelite, 3,300 lb silica flour, 4% bentonite, 2% CaCl) |
| Tail slurry: | 27 bbl silica cement (15.8 lb/gal, 93 sk cement 3,500 lb silica flour, 2% CFR-3) |
| Displacement: | 68 bbl water. No cement returns to surface. |
| Top job #1: | 27 bbl silica cement (100 sk cement, 3,500 lb silica flour, 2% CFR-3, 2% CaCl) |
| Top job #2: | 18 bbl silica cement (47 sk cement, 1,900 lb silica flour, 50 c.f. perlite, 2% CFR-3, 3% bentonite, 3% CaCl) |
| Top job #3 | 18 bbl silica cement (47 sk cement, 1,900 lb silica flour, 50 c.f. perlite, 2% CFR-3, 3% CaCl) |

Theoretical cementing volume: 254 cubic feet; cement required: 778 cubic feet.

BOP equipment was nipped up on July 30 and consisted of:

a. 7 inch ESFO slip-on well head with 2 inch flanged outlets.
b. 6 inch WKM 3M gate valve.
c. 7 inch LWS double-gate preventer with gate and blind rams.
d. High speed rotating head.
e. 2 inch flow and kill lines connected to 2 inch 3M gate valves.

The BOP equipment was pressure tested to 600 psi.

4-1/2 Inch Casing

The cement and 7 inch float equipment were drilled out with a 5-7/8 inch tricone and 5 inch flush joint casing with left-hand buttress threads was set below the wellhead to 1,996 feet to provide a "sleeve" for the core drill rods.

Core drilling with 101mm (3.98" hole x 2.50" core) commenced on July 31 and advanced to 2,505 feet on August 7. Drilling progressed reasonably well with average daily footages of 78 feet per day. At 2,505 feet the hole was cemented back to 2,316 feet with 20 cubic feet of neat cement in an attempt to stabalize a poorly consolidated sandy interval below 2,419 feet. After drilling out cement, the 101mm core hole was advanced to 2,671 feet encountering several poorly consolidated sandy intervals. In an attempt to stabalize the hole, it was cemented back with 20 cubic feet of neat cement. While tripping in the hole on August 13 to drill out cement, several bridged-off intervals were encountered, beginning at 2,205 feet, and drilled out. While cleaning the hole the drill rods became stuck tight while making a connection at 2,234 feet.

A mechanical cutter was tripped in on NQ drill rods (2.75" O.D.) and the 101mm drill rods cut 3 feet above the core barrel. The core barrel assembly dropped down the hole after being cut free from the upper rods but the drill rods would not pull free. The rods were cut at 2,140 feet and finally at 1,995 feet before the upper portion could be pulled free and retrieved. After removing the 5 inch casing sleeve, the remaining 101mm drill rods were recovered by reaming over the rods with a 134mm casing shoe (5.28" O.D. x 4.125" I.D.). The reaming and recovery operation began on August 13 and was completed August 31 (18 days).

After retrieving the 101mm rods, the hole was opened to 5-7/8 inches with a tricone bit from 1,996 - 2,671 feet during a 10 day period from August 31 to September 10. Several zones of poorly consolidated sandy material and fractured unstable formation were encountered and reaming was slow and difficult requiring numerous redrills of unstable intervals. After briefly sticking the drill rods at 2,441 feet while tripping out of the hole, the rotary drill assembly was removed and drilling continued with a 134mm coring assembly (5.28" hole x 3.35" core).

The 134mm core hole was advanced from 2,671 - 3,022 feet in difficult conditions. While drilling the 134mm hole, average core runs were only 5.83 feet and core recovery averaged 87 percent. Due to the hard, fractured, abrasive and unstable nature of this interval, seven bits were consumed in coring 351 feet. Average bit life was slightly over 50 feet. These events resulted in an extremely high bit cost of $34.42 per foot for the 134mm cored interval.

After completing the hole to 3,022 feet, a casing string was run to TD and consisted of: 1,017 feet of flush joint 4-1/2 inch, 11.6 pound/foot J-55 casing from 3,022 - 2,005 feet and short threaded and coupled 4-1/2 inch, 10.5 pound/foot J-55 casing from 2,005 feet to the surface. A guide shoe and float collar were run with the casing. The bottom 200 feet of the casing was cemented with neat cement on September 22.

HQ & NQ Core Drilling (3,022 - 5,526 feet)

Core drilling resumed with HQWL (3.83" hole x 2.50" core) in broken, unstable and abrasive hyaloclastics, basalt flows and intrusive rock from 3,022 - 4,325 feet. Drilling this 1,303 foot interval required 49 days, an average of 26.6 feet per day. The entire interval proved to be extremely difficult to core drill. Core runs in this interval averaged only 3.93 feet, core recovery dropped to 80.49 percent and 31 bits were consumed.

The hole was reduced to NQ (2.98" hole x 1.875" core) and cored from 4,325 - 4,880 feet with similar problems to those encountered while coring with HQ. This 555 foot section required an additional 24 days, an average of 23.1 feet per day. Core runs in this interval averaged 3.54 feet, core recovery averaged 88.62 percent and 6 more bits were consumed.

By contrast, HQ and NQ core drilling the 3,562 foot interval below 3,000 feet in SOH-4 averaged 71.2 feet per day during a 50 day period using only 7 bits (487 feet per bit) with mostly 10 foot core runs and nearly 100 percent core recovery. The problems hampering the core drilling efforts in SOH-1 are discussed below:

a. Short bit life: 31 HQ and 7 NQ bits were expended in drilling 1,649 feet. Average bit footage was 43.4 feet. Each bit change necessiated the time consuming and nonproductive process of tripping all drill rods out of the hole, replacing the bit and tripping back in the hole. In this interval the time involved was 5 - 7 hours, exclusive of cleaning and reaming the hole. The primary reason for short bit life was the pervasively fractured, hard and abrasive nature of the formation.

The fractured rock was generally broken into small (less than 3 inches) angular fragments which tended to roll around below, outside and inside the bit cutting surfaces. This action greatly accelerated deterioration of the bits inner and outer guage. When inside bit guage is lost, the core is unable to slide into the inner tube assembly. Loss of outside gauge made it necessary to spend time reaming the next bit through the undersized hole. The reaming process also caused considerable wear on the bit before any new hole was drilled.

b. Short core runs: The equipment used was designed to retrieve 10 foot sections of core. In this interval the average core retrieval was only 3.93 feet with NQ and 3.54 feet with HQ. Retrieval involves lowering an overshot attached to a 3/8 inch wireline until it latches onto the inner tube assembly, then pulling the inner tube to the surface and lowering an empty tube into position. The time involved depends on the hole depth, in this interval the retrieval operation required 20 - 30 minutes. If, for example, 10 short runs take place in a day, approximately 5 hours of time is lost to non-drilling core retrieval operations.

A ratcheting core barrel assembly was employed while coring HQ and produced a slight improvement in core runs. The ratcheting core barrel has a spring loaded ratchet device which engages when core entering the inner tube blocks off. When engaged it transmits a rapid series of sharp blows to the tube, hopefully, loosening the blockage.

c. Redrilling: The fractured, poorly consolidated rock above 4,880 feet proved to be unstable, with frequent caving. In order to clean the cave and material dropped from the inner tube, redrilling was required after most core runs to clean and stabalize the well bore. Since the core bit is not designed to efficiently grind up loose rubble, a small tricone bit was tripped in on five occassions to clean and stabalize the hole between 4,364 and 4,880 feet. Use of the tricone was successful in cleaning the hole but required additional trips in and out of the hole, which together with cleaning and reaming, often consumed over 24 hours of rig time.

d. Dropped core: The small size of the fractured rock often made it difficult to retain all of the rubble in the inner tube upon retrieval. Occasionally, a piece of this rock would wedge in the drill rods and prevent the empty inner tube from dropping into place. This would force the pulling of drill rods to clear the obstruction. Each trip resulted in the loss of up to 7 hours.

Regarding cost/time effectiveness, the only productive time spent during a core drilling operation is when the bit is on bottom, drilling new hole. Although necessary to continue drilling, time involved in core runs, bit changes, tripping drill rods, reaming and washing the hole, etc. is non-productive in terms of deepening the hole. As the above discussion illustrates, the majority of time in the 3,231 - 4,880 foot interval was consumed by non-coring operations.

Conditions for core drilling above 4,880 feet were extremely difficult and although the progress was slow and expensive, it is a tribute to the Tonto drilling crew that they were able to advance the hole in the adverse drilling environment.

Reasons for the hard, fractured and poorly consolidated nature of the formation are open for suggestion. An obvious correlation in SOH-4, SOH-1 and currently in SOH-2 indicate that the subaerial volcanics provide no significant problems to core drilling. Submarine volcanics and associated clastic material, however, create the hostile enviornment for core drilling described above. This environment presists until a depth is reached where substantial thermal alteration has taken place. Thermal alteration appears to decrease the abrasiveness and secondary mineralization and alteration bonds the fractured and poorly consolidated rock to a state of competence where core drilling can be efficiently accomplished. If this can be expected with regularity in the rift zone, core drilling should be avoided in the interval of submarine volcanics above the zone of thermal alteration.

The subaerial/submarine interface becomes deeper at locations inland with higher elevation. At SOH-4, with a surface elevation of 1,195 feet, the contact is at approximately 4,000 feet below sea level (5,554 ft. G.L.). At SOH-1 the surface elevation is 620 feet and the contact is at 1,831 feet below sea level (2,451 ft. G.L.). At the current hole, SOH-2, situated at an elevation of 270 feet, the contact is approximately 1,380 feet below sea level (1,680 ft. G.L.).

A deeper subaerial/submarine contact provides better opprotunity for thermal alteration and mineralization. With this simple model, continuous coring appears to be most feasable at higher elevation sites along the rift zone as at SOH-4 and the planned SOH-3 hole. Regardless of the location, core drilling from the surface to the subaerial/submarine contact has proved to be feasible and provides valuable information for researchers. Rotary drilling is the most effective method for penetrating the interval of submarine volcanics and hyaloclastic material above the zone of thermal alternation. After casing this interval off, core drilling can resume with reasonable efficiency.

Noise Mitigation And Local Resident Complaints

Noise generated by drilling activities has been a major concern to nearby residents. To underscore this concern, Hawaii County restrictions accompanying the drilling permit limit noise levels at the nearest residence (in some instances slightly more than 1/4 mile) to 55 dBA during daylight hours and 45 dBA at night (7 PM - 7 AM). Although these levels have not been exceeded in 14 months of drilling operations, complaints are often filed simply because a resident can hear noise generated by the operation regardless of measured noise levels. During certain meteorological conditions, noise originating at the SOH site are audible at considerable distances from the site. Although it is not possible for the drilling operations to be completely inaudible, one of the SOH project's target goals is to eliminate even this nuisance level of noise.

Forty complaints were received while drilling SOH-1 (Table 3). Of these, thirty-eight were for noise, one for light and one for odor. Thirty of the complaints were from a single individual located over 1/2 mile from the drill site. All but one of the complaints were from individuals publicly opposed to geothermal development.

To minimize the potential nuisance impact of noises generated by round-the-clock drilling operations, the contractor made extensive modifications and additions to the equipment. Additional sound mitigation measures have been undertaken by Tonto and SOH personnel since the project began. Some of the measures include:

a. Completely enclosing the main power plant, a 410 HP General Motors diesel unit, with sound dampening panels.

b. Constructing sound absorbing duct work over air intake and discharge areas around the engine compartment.

c. Modification of ancillary equipment normally powered by small gas or disel engines. These are now driven by hydraulic motors, powered by the drilling rigs hydraulic system.

d. Enclosing the main hydraulic winch at the top of the mast with sound dampening panels.

e. Erecting sound dampening panels around the front of the drill rig and adjacent to other sources of excessive noise as they are isolated.

d. Lining pipe rack slides with plywood to dampen noise as pipe and casing is lifted to the rig floor.

e. Enclosing the rig floor with heavy wind walls and doors.

f. Installation of large "hospital type" mufflers on the rig engine.

g. Running equipment at lower speeds during night time operations, when practical, to lower noise levels.

h. Suspension of night time operations when work involves excessive noise such as cementing operations.

As one source of noise is quieted, another is often exposed and each drill site poses a new variety of challenges due to differing topography, proximity to neighbors, etc. Evaluation and improving the sound mitigation measures is an ongoing task which will continue throughout the SOH project.

Ground Water Sampling

The surface elevation at SOH-1 is 620 feet and the static water level was measured at between 615 and 620 feet. On June 18, the 101mm core hole reached a depth of 669 feet. A bottom hole temperature of 79 F was measured and the hole was bailed with a 30 foot long bailer constructed of 2 inch galvanized pipe. Samples were collected after 2 hours, 3 hours and 4.5 hours respectively. Temperature increased slightly as the hole was bailed. Sample #3 had a temperature of 88 F. The samples were submitted for a standard water analysis.

Bottom Hole Temperatures

Core drilling presents an excellent opprotunity to monitor formation temperatures on a real time basis as the hole is drilled. This results from several factors:

a. The low rate at which drilling fluids are pumped during core drilling as opposed to rotary drilling larger holes. Pumping rates for core drilling are 10 - 20 gallons per minute while pump rates for rotary drilling larger holes are several hundred gallons per minute. Thus, even when all fluids flow into the formation surrounding the bore hole, the cooling effect is much less when core drilling then rotary drilling and temperature increases are more likely to be noted.

b. Annular space between the well bore and drill rods is less than 0.15 inch in a core hole as opposed to several inches in rotary holes.

c. The relatively thin walled core drill rods rapidly equillibrate to surrounding fluid temperatures, whereas, massive drill collars run behind rotary drill bits require a considerable period of time to reach thermal equillibration.

In order to anticipate potential safety problems related to formation tempertures, bottom hole temperature measurements are taken at intervals of approximately 50 feet. Since the SOH holes are not hampered by requirements of production casing design, additional casing strings can be set as required by changing down hole conditions. Measured bottom hole temperatures will deviate from actural formation temperatures depending on drilling fluid loss into the formation, pump rates, hole size and time of measurement after cessation of pumping.

Tables & Figures

Table 1.
SOH-1 Drilling Summary

| Dates | Day # | Activity |
|---|---|---|
| 5/26 - 5/30 | | Move equipment to site, rig up install water line. |
| 5/31 - 6/2 | 1 - 2 | Core 101mm 0 - 202 ft |
| 6/2 - 6/4 | 3 - 5 | Open hole to 12-1/4" 0 - 202 ft. |
| 6/4 - 6/8 | 5 - 9 | Run 9-5/8" casing, cement and nipple up BOP equipment. |
| 6/9 - 6/14 | 10 - 15 | Stand by for decision from Hawaii County for approval to continue. |
| 6/14 - 7/1 | 15 - 32 | Core 101mm from 202 - 1,996 ft & run deviation survey. |
| 7/2 - 7/25 | 33 - 56 | Open hole to 8-1/2" 202 - 1,996 ft. |
| 7/25 - 7/30 | 56 - 61 | Run 7" casing, drop casing and fish out, cement and nipple up BOP equipment. |
| 7/31 - 8/13 | 62 - 75 | Core 101mm from 1,996 - 2,671 ft. Stick drill rods. |
| 8/13 - 8/31 | 75 - 93 | Fish and ream over 101 rods with 134mm bit and retrieve equipment. |
| 8/31 - 9/10 | 93 - 103 | Open hole to 5-7/8" from 1,996 - 2,671 ft. |
| 9/10 - 9/20 | 103 - 113 | Core 134mm from 2,671 - 3,022 ft. |
| 9/21 - 9/22 | 114 - 115 | Run 4-1/2" casing to 3,022 ft. and cement. |
| 9/22 - 11/10 | 115 - 164 | Core HQ from 3,022 - 4,325 ft. |
| 11/11 - 12/21 | 165 - 205 | Reduce to NQ, core 4,325 - 5,526 ft. |
| 12/22 - 1/2 | N/A N/A | Christmas break. |
| 1/3 - 1/13 | 206 - 217 | Condition hole, run tubing, log, test and rig down. |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 31-May | 101mm | 0.0 | 11.0 | 11.0 | 6.0 | 55% |
| 31-May | 101mm | 11.0 | 21.0 | 10.0 | 10.0 | 100% |
| 31-May | 101mm | 21.0 | 31.0 | 10.0 | 10.0 | 100% |
| 31-May | 101mm | 31.0 | 41.0 | 10.0 | 10.0 | 100% |
| 31-May | 101mm | 41.0 | 52.0 | 11.0 | 10.0 | 91% |
| 31-May | 101mm | 52.0 | 62.0 | 10.0 | 6.0 | 60% |
| 31-May | 101mm | 62.0 | 72.0 | 10.0 | 9.0 | 90% |
| 31-May | 101mm | 62.0 | 72.0 | 10.0 | 9.0 | 90% |
| 31-May | 101mm | 72.0 | 82.0 | 10.0 | 10.0 | 100% |
| 31-May | 101mm | 82.0 | 92.0 | 10.0 | 8.0 | 80% |
| 31-May | 101mm | 92.0 | 102.0 | 10.0 | 10.0 | 100% |
| 31-May | 101mm | 102.0 | 112.0 | 10.0 | 10.0 | 100% |
| 31-May | 101mm | 112.0 | 122.0 | 10.0 | 10.0 | 100% |
| 01-Jun | 101mm | 122.0 | 132.0 | 10.0 | 10.0 | 100% |
| 01-Jun | 101mm | 132.0 | 142.0 | 10.0 | 10.0 | 100% |
| 01-Jun | 101mm | 142.0 | 152.0 | 10.0 | 9.5 | 95% |
| 01-Jun | 101mm | 152.0 | 162.0 | 10.0 | 10.0 | 100% |
| 01-Jun | 101mm | 162.0 | 170.0 | 8.0 | 6.0 | 75% |
| 01-Jun | 101mm | 170.0 | 176.0 | 6.0 | 6.0 | 100% |
| 01-Jun | 101mm | 176.0 | 182.0 | 6.0 | 6.0 | 100% |
| 01-Jun | 101mm | 182.0 | 192.0 | 10.0 | 10.0 | 100% |
| 01-Jun | 101mm | 192.0 | 202.0 | 10.0 | 10.0 | 100% |
| 14-Jun | 101mm | 202.0 | 208.0 | 6.0 | 6.0 | 100% |
| 14-Jun | 101mm | 208.0 | 218.0 | 10.0 | 10.0 | 100% |
| 14-Jun | 101mm | 218.0 | 228.0 | 10.0 | 10.0 | 100% |
| 14-Jun | 101mm | 228.0 | 238.0 | 10.0 | 9.5 | 95% |
| 14-Jun | 101mm | 238.0 | 248.0 | 10.0 | 10.0 | 100% |
| 14-Jun | 101mm | 248.0 | 252.0 | 4.0 | 4.0 | 100% |
| 14-Jun | 101mm | 252.0 | 258.0 | 6.0 | 6.0 | 100% |
| 14-Jun | 101mm | 258.0 | 265.0 | 7.0 | 6.5 | 93% |
| 14-Jun | 101mm | 265.0 | 276.0 | 11.0 | 10.0 | 91% |
| 14-Jun | 101mm | 276.0 | 287.0 | 11.0 | 10.0 | 91% |
| 14-Jun | 101mm | 287.0 | 290.0 | 3.0 | 3.0 | 100% |
| 15-Jun | 101mm | 290.0 | 300.0 | 10.0 | 10.0 | 100% |
| 15-Jun | 101mm | 300.0 | 307.0 | 7.0 | 7.0 | 100% |
| 15-Jun | 101mm | 307.0 | 311.5 | 4.5 | 2.5 | 56% |
| 15-Jun | 101mm | 311.5 | 314.0 | 2.5 | 2.5 | 100% |
| 15-Jun | 101mm | 314.0 | 320.0 | 6.0 | 6.0 | 100% |
| 15-Jun | 101mm | 320.0 | 326.0 | 6.0 | 5.5 | 92% |
| 15-Jun | 101mm | 326.0 | 334.0 | 8.0 | 7.5 | 94% |
| 15-Jun | 101mm | 334.0 | 339.0 | 5.0 | 3.0 | 60% |
| 15-Jun | 101mm | 339.0 | 346.0 | 7.0 | 7.0 | 100% |
| 15-Jun | 101mm | 346.0 | 353.0 | 7.0 | 7.0 | 100% |
| 15-Jun | 101mm | 353.0 | 359.0 | 6.0 | 4.5 | 75% |
| 15-Jun | 101mm | 359.0 | 366.0 | 7.0 | 7.0 | 100% |
| 15-Jun | 101mm | 366.0 | 371.0 | 5.0 | 2.5 | 50% |
| 15-Jun | 101mm | 371.0 | 381.0 | 10.0 | 8.0 | 80% |
| 15-Jun | 101mm | 381.0 | 387.0 | 6.0 | 6.0 | 100% |
| 15-Jun | 101mm | 387.0 | 395.0 | 8.0 | 8.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 15-Jun | 101mm | 395.0 | 405.0 | 10.0 | 10.0 | 100% |
| 15-Jun | 101mm | 405.0 | 414.0 | 9.0 | 7.5 | 83% |
| 15-Jun | 101mm | 414.0 | 425.0 | 11.0 | 9.0 | 82% |
| 15-Jun | 101mm | 425.0 | 433.0 | 8.0 | 6.5 | 81% |
| 16-Jun | 101mm | 433.0 | 441.0 | 8.0 | 7.5 | 94% |
| 16-Jun | 101mm | 441.0 | 448.0 | 7.0 | 6.5 | 93% |
| 16-Jun | 101mm | 448.0 | 451.0 | 3.0 | 3.0 | 100% |
| 16-Jun | 101mm | 451.0 | 460.0 | 9.0 | 9.0 | 100% |
| 16-Jun | 101mm | 460.0 | 470.0 | 10.0 | 10.0 | 100% |
| 16-Jun | 101mm | 470.0 | 475.0 | 5.0 | 4.5 | 90% |
| 16-Jun | 101mm | 475.0 | 484.0 | 9.0 | 9.0 | 100% |
| 16-Jun | 101mm | 484.0 | 487.5 | 3.5 | 3.0 | 86% |
| 16-Jun | 101mm | 487.5 | 490.5 | 3.0 | 1.5 | 50% |
| 16-Jun | 101mm | 490.5 | 493.5 | 3.0 | 3.0 | 100% |
| 16-Jun | 101mm | 493.5 | 498.0 | 4.5 | 3.0 | 67% |
| 16-Jun | 101mm | 498.0 | 503.0 | 5.0 | 3.0 | 60% |
| 16-Jun | 101mm | 503.0 | 513.0 | 10.0 | 10.0 | 100% |
| 16-Jun | 101mm | 513.0 | 518.0 | 5.0 | 3.0 | 60% |
| 16-Jun | 101mm | 518.0 | 528.0 | 10.0 | 8.5 | 85% |
| 16-Jun | 101mm | 528.0 | 534.5 | 6.5 | 4.5 | 69% |
| 16-Jun | 101mm | 534.5 | 539.0 | 4.5 | 3.5 | 78% |
| 16-Jun | 101mm | 539.0 | 549.0 | 10.0 | 9.0 | 90% |
| 16-Jun | 101mm | 549.0 | 556.0 | 7.0 | 7.0 | 100% |
| 16-Jun | 101mm | 556.0 | 563.0 | 7.0 | 10.0 | 143% |
| 17-Jun | 101mm | 563.0 | 573.0 | 10.0 | 8.0 | 80% |
| 17-Jun | 101mm | 573.0 | 576.0 | 3.0 | 2.5 | 83% |
| 17-Jun | 101mm | 576.0 | 583.0 | 7.0 | 7.0 | 100% |
| 17-Jun | 101mm | 583.0 | 589.0 | 6.0 | 6.0 | 100% |
| 17-Jun | 101mm | 589.0 | 592.0 | 3.0 | 3.0 | 100% |
| 17-Jun | 101mm | 592.0 | 594.5 | 2.5 | 2.5 | 100% |
| 17-Jun | 101mm | 594.5 | 602.0 | 7.5 | 6.5 | 87% |
| 17-Jun | 101mm | 602.0 | 610.0 | 8.0 | 7.5 | 94% |
| 17-Jun | 101mm | 610.0 | 616.0 | 6.0 | 6.0 | 100% |
| 17-Jun | 101mm | 616.0 | 622.0 | 6.0 | 6.0 | 100% |
| 17-Jun | 101mm | 622.0 | 631.0 | 9.0 | 8.0 | 89% |
| 17-Jun | 101mm | 631.0 | 639.0 | 8.0 | 8.0 | 100% |
| 17-Jun | 101mm | 639.0 | 647.0 | 8.0 | 8.0 | 100% |
| 17-Jun | 101mm | 647.0 | 657.0 | 10.0 | 6.0 | 60% |
| 17-Jun | 101mm | 657.0 | 665.0 | 8.0 | 4.5 | 56% |
| 17-Jun | 101mm | 665.0 | 669.0 | 4.0 | 4.0 | 100% |
| 18-Jun | 101mm | 669.0 | 675.0 | 6.0 | 5.0 | 83% |
| 18-Jun | 101mm | 675.0 | 681.0 | 6.0 | 5.0 | 83% |
| 18-Jun | 101mm | 681.0 | 691.0 | 10.0 | 10.0 | 100% |
| 18-Jun | 101mm | 691.0 | 701.0 | 10.0 | 8.5 | 85% |
| 18-Jun | 101mm | 701.0 | 710.5 | 9.5 | 9.0 | 95% |
| 18-Jun | 101mm | 710.5 | 714.5 | 4.0 | 3.0 | 75% |
| 18-Jun | 101mm | 714.5 | 717.0 | 2.5 | 0.0 | 0% |
| 18-Jun | 101mm | 717.0 | 719.5 | 2.5 | 2.5 | 100% |
| 18-Jun | 101mm | 719.5 | 720.5 | 1.0 | 1.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 18-Jun | 101mm | 720.5 | 723.0 | 2.5 | 1.0 | 40% |
| 18-Jun | 101mm | 723.0 | 730.0 | 7.0 | 4.5 | 64% |
| 18-Jun | 101mm | 730.0 | 732.0 | 2.0 | 1.0 | 50% |
| 18-Jun | 101mm | 732.0 | 739.0 | 7.0 | 3.5 | 50% |
| 18-Jun | 101mm | 739.0 | 749.0 | 10.0 | 10.0 | 100% |
| 18-Jun | 101mm | 749.0 | 755.0 | 6.0 | 6.0 | 100% |
| 19-Jun | 101mm | 755.0 | 761.0 | 6.0 | 4.0 | 67% |
| 19-Jun | 101mm | 761.0 | 766.0 | 5.0 | 2.0 | 40% |
| 19-Jun | 101mm | 766.0 | 772.5 | 6.5 | 6.5 | 100% |
| 19-Jun | 101mm | 772.5 | 779.0 | 6.5 | 4.5 | 69% |
| 19-Jun | 101mm | 779.0 | 780.5 | 1.5 | 0.5 | 33% |
| 19-Jun | 101mm | 780.5 | 788.5 | 8.0 | 7.0 | 88% |
| 19-Jun | 101mm | 788.5 | 792.5 | 4.0 | 3.5 | 88% |
| 19-Jun | 101mm | 792.5 | 803.0 | 10.5 | 7.0 | 67% |
| 19-Jun | 101mm | 803.0 | 813.0 | 10.0 | 9.0 | 90% |
| 19-Jun | 101mm | 813.0 | 817.5 | 4.5 | 4.5 | 100% |
| 19-Jun | 101mm | 817.5 | 820.0 | 2.5 | 2.5 | 100% |
| 19-Jun | 101mm | 820.0 | 829.0 | 9.0 | 8.0 | 89% |
| 19-Jun | 101mm | 829.0 | 839.0 | 10.0 | 10.0 | 100% |
| 19-Jun | 101mm | 839.0 | 843.0 | 4.0 | 2.5 | 63% |
| 19-Jun | 101mm | 843.0 | 853.0 | 10.0 | 6.5 | 65% |
| 19-Jun | 101mm | 853.0 | 857.5 | 4.5 | 4.0 | 89% |
| 19-Jun | 101mm | 857.5 | 866.0 | 8.5 | 7.0 | 82% |
| 19-Jun | 101mm | 866.0 | 870.0 | 4.0 | 2.5 | 63% |
| 19-Jun | 101mm | 870.0 | 874.0 | 4.0 | 3.5 | 88% |
| 20-Jun | 101mm | 874.0 | 885.0 | 11.0 | 10.0 | 91% |
| 20-Jun | 101mm | 885.0 | 894.0 | 9.0 | 9.0 | 100% |
| 20-Jun | 101mm | 894.0 | 899.0 | 5.0 | 3.0 | 60% |
| 20-Jun | 101mm | 899.0 | 904.0 | 5.0 | 5.0 | 100% |
| 20-Jun | 101mm | 904.0 | 911.0 | 7.0 | 5.0 | 71% |
| 20-Jun | 101mm | 911.0 | 921.0 | 10.0 | 10.0 | 100% |
| 20-Jun | 101mm | 921.0 | 931.0 | 10.0 | 9.0 | 90% |
| 20-Jun | 101mm | 931.0 | 934.0 | 3.0 | 3.0 | 100% |
| 20-Jun | 101mm | 934.0 | 936.0 | 2.0 | 2.0 | 100% |
| 20-Jun | 101mm | 936.0 | 944.0 | 8.0 | 6.0 | 75% |
| 20-Jun | 101mm | 944.0 | 950.5 | 6.5 | 6.0 | 92% |
| 20-Jun | 101mm | 950.5 | 956.5 | 6.0 | 4.0 | 67% |
| 20-Jun | 101mm | 956.5 | 962.0 | 5.5 | 5.5 | 100% |
| 20-Jun | 101mm | 962.0 | 971.0 | 9.0 | 7.5 | 83% |
| 20-Jun | 101mm | 971.0 | 976.0 | 5.0 | 4.0 | 80% |
| 20-Jun | 101mm | 976.0 | 984.0 | 8.0 | 7.0 | 88% |
| 21-Jun | 101mm | 984.0 | 989.0 | 5.0 | 5.0 | 100% |
| 21-Jun | 101mm | 989.0 | 994.0 | 5.0 | 5.0 | 100% |
| 21-Jun | 101mm | 994.0 | 1,000.0 | 6.0 | 6.0 | 100% |
| 21-Jun | 101mm | 1,000.0 | 1,006.0 | 6.0 | 6.0 | 100% |
| 21-Jun | 101mm | 1,006.0 | 1,009.5 | 3.5 | 3.5 | 100% |
| 21-Jun | 101mm | 1,009.5 | 1,010.0 | 0.5 | 0.5 | 100% |
| 21-Jun | 101mm | 1,010.0 | 1,015.0 | 5.0 | 5.0 | 100% |
| 21-Jun | 101mm | 1,015.0 | 1,025.0 | 10.0 | 10.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 21-Jun | 101mm | 1,025.0 | 1,029.0 | 4.0 | 3.5 | 88% |
| 21-Jun | 101mm | 1,029.0 | 1,034.0 | 5.0 | 5.0 | 100% |
| 21-Jun | 101mm | 1,034.0 | 1,036.0 | 2.0 | 2.0 | 100% |
| 21-Jun | 101mm | 1,036.0 | 1,040.0 | 4.0 | 4.0 | 100% |
| 22-Jun | 101mm | 1,040.0 | 1,048.0 | 8.0 | 5.0 | 63% |
| 22-Jun | 101mm | 1,048.0 | 1,051.0 | 3.0 | 3.0 | 100% |
| 22-Jun | 101mm | 1,051.0 | 1,055.0 | 4.0 | 4.0 | 100% |
| 22-Jun | 101mm | 1,055.0 | 1,059.0 | 4.0 | 2.0 | 50% |
| 22-Jun | 101mm | 1,059.0 | 1,065.0 | 6.0 | 6.0 | 100% |
| 22-Jun | 101mm | 1,065.0 | 1,071.0 | 6.0 | 6.0 | 100% |
| 22-Jun | 101mm | 1,071.0 | 1,072.5 | 1.5 | 1.5 | 100% |
| 22-Jun | 101mm | 1,072.5 | 1,077.5 | 5.0 | 5.0 | 100% |
| 22-Jun | 101mm | 1,077.5 | 1,087.0 | 9.5 | 9.5 | 100% |
| 22-Jun | 101mm | 1,087.0 | 1,094.0 | 7.0 | 3.0 | 43% |
| 22-Jun | 101mm | 1,094.0 | 1,100.0 | 6.0 | 6.0 | 100% |
| 22-Jun | 101mm | 1,100.0 | 1,107.0 | 7.0 | 6.0 | 86% |
| 22-Jun | 101mm | 1,107.0 | 1,112.0 | 5.0 | 3.0 | 60% |
| 22-Jun | 101mm | 1,112.0 | 1,115.0 | 3.0 | 2.0 | 67% |
| 22-Jun | 101mm | 1,115.0 | 1,123.0 | 8.0 | 7.5 | 94% |
| 22-Jun | 101mm | 1,123.0 | 1,128.0 | 5.0 | 3.5 | 70% |
| 22-Jun | 101mm | 1,128.0 | 1,136.5 | 8.5 | 8.0 | 94% |
| 22-Jun | 101mm | 1,136.5 | 1,142.0 | 5.5 | 2.5 | 45% |
| 23-Jun | 101mm | 1,142.0 | 1,148.0 | 6.0 | 4.0 | 67% |
| 23-Jun | 101mm | 1,148.0 | 1,156.0 | 8.0 | 4.0 | 50% |
| 23-Jun | 101mm | 1,156.0 | 1,163.0 | 7.0 | 5.0 | 71% |
| 23-Jun | 101mm | 1,163.0 | 1,165.0 | 2.0 | 1.5 | 75% |
| 23-Jun | 101mm | 1,165.0 | 1,169.5 | 4.5 | 3.0 | 67% |
| 23-Jun | 101mm | 1,169.5 | 1,176.5 | 7.0 | 6.0 | 86% |
| 23-Jun | 101mm | 1,176.5 | 1,180.0 | 3.5 | 3.0 | 86% |
| 23-Jun | 101mm | 1,180.0 | 1,184.5 | 4.5 | 4.5 | 100% |
| 23-Jun | 101mm | 1,184.5 | 1,188.5 | 4.0 | 3.0 | 75% |
| 23-Jun | 101mm | 1,188.5 | 1,193.0 | 4.5 | 3.5 | 78% |
| 23-Jun | 101mm | 1,193.0 | 1,198.0 | 5.0 | 4.5 | 90% |
| 23-Jun | 101mm | 1,198.0 | 1,206.0 | 8.0 | 7.0 | 88% |
| 23-Jun | 101mm | 1,206.0 | 1,213.0 | 7.0 | 7.0 | 100% |
| 23-Jun | 101mm | 1,213.0 | 1,215.0 | 2.0 | 1.5 | 75% |
| 23-Jun | 101mm | 1,215.0 | 1,220.5 | 5.5 | 5.0 | 91% |
| 23-Jun | 101mm | 1,220.5 | 1,222.0 | 1.5 | 1.0 | 67% |
| 23-Jun | 101mm | 1,222.0 | 1,227.5 | 5.5 | 5.0 | 91% |
| 23-Jun | 101mm | 1,227.5 | 1,233.0 | 5.5 | 5.0 | 91% |
| 23-Jun | 101mm | 1,233.0 | 1,241.0 | 8.0 | 7.0 | 88% |
| 23-Jun | 101mm | 1,241.0 | 1,245.0 | 4.0 | 4.0 | 100% |
| 24-Jun | 101mm | 1,245.0 | 1,256.0 | 11.0 | 10.0 | 91% |
| 24-Jun | 101mm | 1,256.0 | 1,266.0 | 10.0 | 10.0 | 100% |
| 24-Jun | 101mm | 1,266.0 | 1,268.0 | 2.0 | 1.0 | 50% |
| 24-Jun | 101mm | 1,268.0 | 1,271.0 | 3.0 | 3.0 | 100% |
| 24-Jun | 101mm | 1,271.0 | 1,274.0 | 3.0 | 1.5 | 50% |
| 24-Jun | 101mm | 1,274.0 | 1,278.0 | 4.0 | 4.0 | 100% |
| 24-Jun | 101mm | 1,278.0 | 1,281.5 | 3.5 | 3.5 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 24-Jun | 101mm | 1,281.5 | 1,285.0 | 3.5 | 3.0 | 86% |
| 24-Jun | 101mm | 1,285.0 | 1,290.0 | 5.0 | 5.0 | 100% |
| 24-Jun | 101mm | 1,290.0 | 1,295.0 | 5.0 | 4.5 | 90% |
| 24-Jun | 101mm | 1,295.0 | 1,301.0 | 6.0 | 5.0 | 83% |
| 24-Jun | 101mm | 1,301.0 | 1,306.5 | 5.5 | 5.0 | 91% |
| 24-Jun | 101mm | 1,306.5 | 1,317.0 | 10.5 | 10.0 | 95% |
| 24-Jun | 101mm | 1,317.0 | 1,322.0 | 5.0 | 4.0 | 80% |
| 24-Jun | 101mm | 1,322.0 | 1,330.0 | 8.0 | 8.0 | 100% |
| 24-Jun | 101mm | 1,330.0 | 1,334.0 | 4.0 | 2.5 | 63% |
| 25-Jun | 101mm | 1,334.0 | 1,337.0 | 3.0 | 3.0 | 100% |
| 25-Jun | 101mm | 1,337.0 | 1,346.0 | 9.0 | 9.0 | 100% |
| 25-Jun | 101mm | 1,346.0 | 1,348.0 | 2.0 | 0.0 | 0% |
| 25-Jun | 101mm | 1,348.0 | 1,357.0 | 9.0 | 9.0 | 100% |
| 25-Jun | 101mm | 1,357.0 | 1,360.0 | 3.0 | 3.0 | 100% |
| 25-Jun | 101mm | 1,360.0 | 1,370.0 | 10.0 | 10.0 | 100% |
| 25-Jun | 101mm | 1,370.0 | 1,380.0 | 10.0 | 10.0 | 100% |
| 25-Jun | 101mm | 1,380.0 | 1,384.0 | 4.0 | 2.5 | 63% |
| 25-Jun | 101mm | 1,384.0 | 1,390.0 | 6.0 | 6.0 | 100% |
| 25-Jun | 101mm | 1,390.0 | 1,394.0 | 4.0 | 2.5 | 63% |
| 25-Jun | 101mm | 1,394.0 | 1,398.5 | 4.5 | 4.0 | 89% |
| 25-Jun | 101mm | 1,398.5 | 1,402.0 | 3.5 | 2.0 | 57% |
| 25-Jun | 101mm | 1,402.0 | 1,411.0 | 9.0 | 9.0 | 100% |
| 25-Jun | 101mm | 1,411.0 | 1,414.0 | 3.0 | 3.0 | 100% |
| 25-Jun | 101mm | 1,414.0 | 1,418.0 | 4.0 | 3.0 | 75% |
| 26-Jun | 101mm | 1,418.0 | 1,419.5 | 1.5 | 0.5 | 33% |
| 26-Jun | 101mm | 1,419.5 | 1,423.5 | 4.0 | 3.0 | 75% |
| 26-Jun | 101mm | 1,423.5 | 1,434.0 | 10.5 | 8.0 | 76% |
| 26-Jun | 101mm | 1,434.0 | 1,439.0 | 5.0 | 5.0 | 100% |
| 26-Jun | 101mm | 1,439.0 | 1,446.0 | 7.0 | 6.5 | 93% |
| 26-Jun | 101mm | 1,446.0 | 1,452.5 | 6.5 | 6.5 | 100% |
| 26-Jun | 101mm | 1,452.5 | 1,459.0 | 6.5 | 6.5 | 100% |
| 26-Jun | 101mm | 1,459.0 | 1,465.0 | 6.0 | 6.0 | 100% |
| 26-Jun | 101mm | 1,465.0 | 1,475.0 | 10.0 | 10.0 | 100% |
| 26-Jun | 101mm | 1,475.0 | 1,485.0 | 10.0 | 10.0 | 100% |
| 26-Jun | 101mm | 1,485.0 | 1,495.0 | 10.0 | 8.5 | 85% |
| 26-Jun | 101mm | 1,495.0 | 1,501.0 | 6.0 | 4.0 | 67% |
| 26-Jun | 101mm | 1,501.0 | 1,508.0 | 7.0 | 6.0 | 86% |
| 27-Jun | 101mm | 1,508.0 | 1,515.0 | 7.0 | 7.0 | 100% |
| 27-Jun | 101mm | 1,515.0 | 1,521.0 | 6.0 | 3.5 | 58% |
| 27-Jun | 101mm | 1,521.0 | 1,526.0 | 5.0 | 3.0 | 60% |
| 27-Jun | 101mm | 1,526.0 | 1,533.0 | 7.0 | 6.0 | 86% |
| 27-Jun | 101mm | 1,533.0 | 1,539.0 | 6.0 | 5.0 | 83% |
| 27-Jun | 101mm | 1,539.0 | 1,548.0 | 9.0 | 7.5 | 83% |
| 27-Jun | 101mm | 1,548.0 | 1,557.0 | 9.0 | 8.0 | 89% |
| 27-Jun | 101mm | 1,557.0 | 1,564.0 | 7.0 | 7.0 | 100% |
| 27-Jun | 101mm | 1,564.0 | 1,573.0 | 9.0 | 7.0 | 78% |
| 27-Jun | 101mm | 1,573.0 | 1,578.0 | 5.0 | 4.0 | 80% |
| 27-Jun | 101mm | 1,578.0 | 1,585.0 | 7.0 | 6.0 | 86% |
| 27-Jun | 101mm | 1,585.0 | 1,589.0 | 4.0 | 2.5 | 63% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 27-Jun | 101mm | 1,589.0 | 1,596.0 | 7.0 | 6.0 | 86% |
| 27-Jun | 101mm | 1,596.0 | 1,604.5 | 8.5 | 7.5 | 88% |
| 27-Jun | 101mm | 1,604.5 | 1,615.0 | 10.5 | 10.0 | 95% |
| 28-Jun | 101mm | 1,615.0 | 1,618.0 | 3.0 | 1.0 | 33% |
| 28-Jun | 101mm | 1,618.0 | 1,623.0 | 5.0 | 0.5 | 10% |
| 28-Jun | 101mm | 1,623.0 | 1,633.0 | 10.0 | 10.0 | 100% |
| 28-Jun | 101mm | 1,633.0 | 1,643.0 | 10.0 | 6.0 | 60% |
| 28-Jun | 101mm | 1,643.0 | 1,653.0 | 10.0 | 10.0 | 100% |
| 28-Jun | 101mm | 1,653.0 | 1,655.0 | 2.0 | 1.0 | 50% |
| 28-Jun | 101mm | 1,655.0 | 1,660.0 | 5.0 | 4.5 | 90% |
| 28-Jun | 101mm | 1,660.0 | 1,671.0 | 11.0 | 10.0 | 91% |
| 28-Jun | 101mm | 1,671.0 | 1,681.0 | 10.0 | 8.5 | 85% |
| 28-Jun | 101mm | 1,681.0 | 1,687.5 | 6.5 | 4.5 | 69% |
| 28-Jun | 101mm | 1,687.5 | 1,695.0 | 7.5 | 7.5 | 100% |
| 28-Jun | 101mm | 1,695.0 | 1,702.0 | 7.0 | 6.0 | 86% |
| 28-Jun | 101mm | 1,702.0 | 1,709.0 | 7.0 | 5.0 | 71% |
| 29-Jun | 101mm | 1,709.0 | 1,719.0 | 10.0 | 9.0 | 90% |
| 29-Jun | 101mm | 1,719.0 | 1,729.0 | 10.0 | 9.0 | 90% |
| 29-Jun | 101mm | 1,729.0 | 1,737.0 | 8.0 | 8.0 | 100% |
| 29-Jun | 101mm | 1,737.0 | 1,745.0 | 8.0 | 6.5 | 81% |
| 29-Jun | 101mm | 1,745.0 | 1,750.0 | 5.0 | 2.5 | 50% |
| 29-Jun | 101mm | 1,750.0 | 1,752.0 | 2.0 | 0.0 | 0% |
| 29-Jun | 101mm | 1,752.0 | 1,756.0 | 4.0 | 3.0 | 75% |
| 29-Jun | 101mm | 1,756.0 | 1,764.0 | 8.0 | 8.0 | 100% |
| 29-Jun | 101mm | 1,764.0 | 1,774.0 | 10.0 | 10.0 | 100% |
| 29-Jun | 101mm | 1,774.0 | 1,782.0 | 8.0 | 8.0 | 100% |
| 29-Jun | 101mm | 1,782.0 | 1,792.0 | 10.0 | 10.0 | 100% |
| 29-Jun | 101mm | 1,792.0 | 1,802.0 | 10.0 | 10.0 | 100% |
| 30-Jun | 101mm | 1,802.0 | 1,813.0 | 11.0 | 10.0 | 91% |
| 30-Jun | 101mm | 1,813.0 | 1,823.0 | 10.0 | 10.0 | 100% |
| 30-Jun | 101mm | 1,823.0 | 1,832.0 | 9.0 | 8.5 | 94% |
| 30-Jun | 101mm | 1,832.0 | 1,841.0 | 9.0 | 9.0 | 100% |
| 30-Jun | 101mm | 1,841.0 | 1,851.0 | 10.0 | 10.0 | 100% |
| 30-Jun | 101mm | 1,851.0 | 1,857.0 | 6.0 | 6.0 | 100% |
| 30-Jun | 101mm | 1,857.0 | 1,862.0 | 5.0 | 5.0 | 100% |
| 30-Jun | 101mm | 1,862.0 | 1,872.0 | 10.0 | 10.0 | 100% |
| 30-Jun | 101mm | 1,872.0 | 1,882.0 | 10.0 | 10.0 | 100% |
| 30-Jun | 101mm | 1,882.0 | 1,892.0 | 10.0 | 10.0 | 100% |
| 30-Jun | 101mm | 1,892.0 | 1,902.0 | 10.0 | 10.0 | 100% |
| 30-Jun | 101mm | 1,902.0 | 1,911.0 | 9.0 | 9.0 | 100% |
| 01-Jul | 101mm | 1,911.0 | 1,918.0 | 7.0 | 5.0 | 71% |
| 01-Jul | 101mm | 1,918.0 | 1,921.0 | 3.0 | 3.0 | 100% |
| 01-Jul | 101mm | 1,921.0 | 1,931.0 | 10.0 | 10.0 | 100% |
| 01-Jul | 101mm | 1,931.0 | 1,940.0 | 9.0 | 8.0 | 89% |
| 01-Jul | 101mm | 1,940.0 | 1,946.0 | 6.0 | 6.0 | 100% |
| 01-Jul | 101mm | 1,946.0 | 1,953.0 | 7.0 | 6.0 | 86% |
| 01-Jul | 101mm | 1,953.0 | 1,957.0 | 4.0 | 4.0 | 100% |
| 01-Jul | 101mm | 1,957.0 | 1,960.0 | 3.0 | 3.0 | 100% |
| 01-Jul | 101mm | 1,960.0 | 1,964.0 | 4.0 | 4.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 01-Jul | 101mm | 1,964.0 | 1,967.0 | 3.0 | 2.5 | 83% |
| 01-Jul | 101mm | 1,967.0 | 1,974.0 | 7.0 | 5.0 | 71% |
| 01-Jul | 101mm | 1,974.0 | 1,981.0 | 7.0 | 6.5 | 93% |
| 01-Jul | 101mm | 1,981.0 | 1,990.0 | 9.0 | 7.0 | 78% |
| 01-Jul | 101mm | 1,990.0 | 1,996.0 | 6.0 | 6.0 | 100% |
| 31-Jul | 101mm | 1,996.0 | 1,999.0 | 3.0 | 1.0 | 33% |
| 31-Jul | 101mm | 1,999.0 | 2,003.0 | 4.0 | 4.0 | 100% |
| 31-Jul | 101mm | 2,003.0 | 2,009.0 | 6.0 | 6.0 | 100% |
| 31-Jul | 101mm | 2,009.0 | 2,012.0 | 3.0 | 3.0 | 100% |
| 31-Jul | 101mm | 2,012.0 | 2,014.0 | 2.0 | 1.0 | 50% |
| 01-Aug | 101mm | 2,014.0 | 2,018.0 | 4.0 | 4.0 | 100% |
| 01-Aug | 101mm | 2,018.0 | 2,025.5 | 7.5 | 7.5 | 100% |
| 01-Aug | 101mm | 2,025.5 | 2,030.5 | 5.0 | 5.0 | 100% |
| 01-Aug | 101mm | 2,030.5 | 2,036.5 | 6.0 | 2.5 | 42% |
| 01-Aug | 101mm | 2,036.5 | 2,040.0 | 3.5 | 3.5 | 100% |
| 01-Aug | 101mm | 2,040.0 | 2,048.0 | 8.0 | 8.0 | 100% |
| 01-Aug | 101mm | 2,048.0 | 2,056.0 | 8.0 | 8.0 | 100% |
| 01-Aug | 101mm | 2,056.0 | 2,059.0 | 3.0 | 3.0 | 100% |
| 01-Aug | 101mm | 2,059.0 | 2,060.0 | 1.0 | 0.5 | 50% |
| 01-Aug | 101mm | 2,060.0 | 2,061.5 | 1.5 | 1.0 | 67% |
| 01-Aug | 101mm | 2,061.5 | 2,074.5 | 13.0 | 2.0 | 15% |
| 02-Aug | 101mm | 2,074.5 | 2,080.0 | 5.5 | 5.5 | 100% |
| 02-Aug | 101mm | 2,080.0 | 2,086.5 | 6.5 | 6.5 | 100% |
| 02-Aug | 101mm | 2,086.5 | 2,087.0 | 0.5 | 0.5 | 100% |
| 02-Aug | 101mm | 2,087.0 | 2,097.0 | 10.0 | 10.0 | 100% |
| 02-Aug | 101mm | 2,097.0 | 2,107.0 | 10.0 | 10.0 | 100% |
| 02-Aug | 101mm | 2,107.0 | 2,117.0 | 10.0 | 10.0 | 100% |
| 02-Aug | 101mm | 2,117.0 | 2,127.0 | 10.0 | 10.0 | 100% |
| 02-Aug | 101mm | 2,127.0 | 2,137.0 | 10.0 | 10.0 | 100% |
| 03-Aug | 101mm | 2,137.0 | 2,147.0 | 10.0 | 10.0 | 100% |
| 03-Aug | 101mm | 2,147.0 | 2,157.5 | 10.5 | 10.5 | 100% |
| 03-Aug | 101mm | 2,157.5 | 2,160.0 | 2.5 | 2.5 | 100% |
| 03-Aug | 101mm | 2,160.0 | 2,166.5 | 6.5 | 6.5 | 100% |
| 03-Aug | 101mm | 2,166.5 | 2,176.5 | 10.0 | 10.0 | 100% |
| 03-Aug | 101mm | 2,176.5 | 2,184.0 | 7.5 | 7.5 | 100% |
| 03-Aug | 101mm | 2,184.0 | 2,191.0 | 7.0 | 7.0 | 100% |
| 03-Aug | 101mm | 2,191.0 | 2,201.0 | 10.0 | 10.0 | 100% |
| 03-Aug | 101mm | 2,201.0 | 2,211.0 | 10.0 | 10.0 | 100% |
| 04-Aug | 101mm | 2,211.0 | 2,219.0 | 8.0 | 8.0 | 100% |
| 04-Aug | 101mm | 2,219.0 | 2,224.0 | 5.0 | 5.0 | 100% |
| 04-Aug | 101mm | 2,224.0 | 2,231.0 | 7.0 | 7.0 | 100% |
| 04-Aug | 101mm | 2,231.0 | 2,241.0 | 10.0 | 10.0 | 100% |
| 04-Aug | 101mm | 2,241.0 | 2,251.0 | 10.0 | 10.0 | 100% |
| 04-Aug | 101mm | 2,251.0 | 2,261.0 | 10.0 | 10.0 | 100% |
| 04-Aug | 101mm | 2,261.0 | 2,266.0 | 5.0 | 4.5 | 90% |
| 05-Aug | 101mm | 2,266.0 | 2,273.5 | 7.5 | 7.5 | 100% |
| 05-Aug | 101mm | 2,273.5 | 2,283.5 | 10.0 | 10.0 | 100% |
| 05-Aug | 101mm | 2,283.5 | 2,293.5 | 10.0 | 10.0 | 100% |
| 05-Aug | 101mm | 2,293.5 | 2,304.0 | 10.5 | 10.5 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 05-Aug | 101mm | 2,304.0 | 2,314.0 | 10.0 | 10.0 | 100% |
| 05-Aug | 101mm | 2,314.0 | 2,324.5 | 10.5 | 10.0 | 95% |
| 05-Aug | 101mm | 2,324.5 | 2,331.0 | 6.5 | 6.5 | 100% |
| 05-Aug | 101mm | 2,331.0 | 2,338.0 | 7.0 | 7.0 | 100% |
| 05-Aug | 101mm | 2,338.0 | 2,348.0 | 10.0 | 10.0 | 100% |
| 05-Aug | 101mm | 2,348.0 | 2,358.0 | 10.0 | 10.0 | 100% |
| 05-Aug | 101mm | 2,358.0 | 2,368.0 | 10.0 | 10.0 | 100% |
| 06-Aug | 101mm | 2,368.0 | 2,378.5 | 10.5 | 7.5 | 71% |
| 06-Aug | 101mm | 2,378.5 | 2,388.5 | 10.0 | 10.0 | 100% |
| 06-Aug | 101mm | 2,388.5 | 2,399.0 | 10.5 | 10.5 | 100% |
| 06-Aug | 101mm | 2,399.0 | 2,409.0 | 10.0 | 10.0 | 100% |
| 06-Aug | 101mm | 2,409.0 | 2,419.5 | 10.5 | 10.5 | 100% |
| 06-Aug | 101mm | 2,419.5 | 2,429.5 | 10.0 | 10.0 | 100% |
| 06-Aug | 101mm | 2,429.5 | 2,437.5 | 8.0 | 6.0 | 75% |
| 06-Aug | 101mm | 2,437.5 | 2,448.0 | 10.5 | 0.5 | 5% |
| 06-Aug | 101mm | 2,448.0 | 2,450.0 | 2.0 | 2.0 | 100% |
| 06-Aug | 101mm | 2,450.0 | 2,455.0 | 5.0 | 5.0 | 100% |
| 06-Aug | 101mm | 2,455.0 | 2,465.0 | 10.0 | 10.0 | 100% |
| 06-Aug | 101mm | 2,465.0 | 2,475.0 | 10.0 | 10.0 | 100% |
| 06-Aug | 101mm | 2,475.0 | 2,481.0 | 6.0 | 6.0 | 100% |
| 07-Aug | 101mm | 2,481.0 | 2,491.0 | 10.0 | 10.0 | 100% |
| 07-Aug | 101mm | 2,491.0 | 2,501.0 | 10.0 | 10.0 | 100% |
| 07-Aug | 101mm | 2,501.0 | 2,505.5 | 4.5 | 4.5 | 100% |
| 09-Aug | 101mm | 2,505.5 | 2,510.0 | 4.5 | 4.5 | 100% |
| 09-Aug | 101mm | 2,510.0 | 2,520.0 | 10.0 | 10.0 | 100% |
| 09-Aug | 101mm | 2,520.0 | 2,530.0 | 10.0 | 10.0 | 100% |
| 09-Aug | 101mm | 2,530.0 | 2,540.0 | 10.0 | 10.0 | 100% |
| 10-Aug | 101mm | 2,540.0 | 2,550.0 | 10.0 | 10.0 | 100% |
| 10-Aug | 101mm | 2,550.0 | 2,560.0 | 10.0 | 10.0 | 100% |
| 10-Aug | 101mm | 2,560.0 | 2,569.5 | 9.5 | 9.5 | 100% |
| 10-Aug | 101mm | 2,569.5 | 2,580.0 | 10.5 | 10.5 | 100% |
| 10-Aug | 101mm | 2,580.0 | 2,590.0 | 10.0 | 4.5 | 45% |
| 10-Aug | 101mm | 2,590.0 | 2,600.0 | 10.0 | 10.0 | 100% |
| 10-Aug | 101mm | 2,600.0 | 2,610.0 | 10.0 | 5.0 | 50% |
| 10-Aug | 101mm | 2,610.0 | 2,620.0 | 10.0 | 10.0 | 100% |
| 10-Aug | 101mm | 2,620.0 | 2,629.0 | 9.0 | 9.0 | 100% |
| 10-Aug | 101mm | 2,629.0 | 2,639.0 | 10.0 | 10.0 | 100% |
| 10-Aug | 101mm | 2,639.0 | 2,645.0 | 6.0 | 5.0 | 83% |
| 11-Aug | 101mm | 2,645.0 | 2,655.0 | 10.0 | 10.0 | 100% |
| 11-Aug | 101mm | 2,655.0 | 2,661.0 | 6.0 | 6.0 | 100% |
| 11-Aug | 101mm | 2,661.0 | 2,671.0 | 10.0 | 3.5 | 35% |
| 10-Sep | 134mm | 2,671.0 | 2,679.0 | 8.0 | 8.0 | 100% |
| 10-Sep | 134mm | 2,679.0 | 2,691.0 | 12.0 | 12.0 | 100% |
| 10-Sep | 134mm | 2,691.0 | 2,702.0 | 11.0 | 11.0 | 100% |
| 10-Sep | 134mm | 2,702.0 | 2,708.0 | 6.0 | 6.0 | 100% |
| 10-Sep | 134mm | 2,708.0 | 2,714.0 | 6.0 | 6.0 | 100% |
| 10-Sep | 134mm | 2,714.0 | 2,717.0 | 3.0 | 0.0 | 0% |
| 11-Sep | 134mm | 2,717.0 | 2,721.0 | 4.0 | 4.0 | 100% |
| 11-Sep | 134mm | 2,721.0 | 2,726.0 | 5.0 | 5.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 11-Sep | 134mm | 2,726.0 | 2,730.0 | 4.0 | 4.0 | 100% |
| 11-Sep | 134mm | 2,730.0 | 2,732.0 | 2.0 | 2.0 | 100% |
| 11-Sep | 134mm | 2,732.0 | 2,733.0 | 1.0 | 1.0 | 100% |
| 11-Sep | 134mm | 2,733.0 | 2,738.0 | 5.0 | 5.0 | 100% |
| 12-Sep | 134mm | 2,738.0 | 2,752.0 | 14.0 | 5.0 | 36% |
| 12-Sep | 134mm | 2,752.0 | 2,755.0 | 3.0 | 3.0 | 100% |
| 12-Sep | 134mm | 2,755.0 | 2,758.0 | 3.0 | 0.0 | 0% |
| 12-Sep | 134mm | 2,758.0 | 2,763.0 | 5.0 | 1.0 | 20% |
| 12-Sep | 134mm | 2,763.0 | 2,768.0 | 5.0 | 0.0 | 0% |
| 12-Sep | 134mm | 2,768.0 | 2,770.0 | 2.0 | 2.0 | 100% |
| 13-Sep | 134mm | 2,770.0 | 2,782.0 | 12.0 | 12.0 | 100% |
| 13-Sep | 134mm | 2,782.0 | 2,793.0 | 11.0 | 11.0 | 100% |
| 13-Sep | 134mm | 2,793.0 | 2,805.0 | 12.0 | 12.0 | 100% |
| 13-Sep | 134mm | 2,805.0 | 2,816.0 | 11.0 | 11.0 | 100% |
| 13-Sep | 134mm | 2,816.0 | 2,827.0 | 11.0 | 11.0 | 100% |
| 13-Sep | 134mm | 2,827.0 | 2,836.0 | 9.0 | 9.0 | 100% |
| 14-Sep | 134mm | 2,836.0 | 2,846.0 | 10.0 | 6.0 | 60% |
| 14-Sep | 134mm | 2,846.0 | 2,851.0 | 5.0 | 1.0 | 20% |
| 14-Sep | 134mm | 2,851.0 | 2,852.0 | 1.0 | 0.0 | 0% |
| 14-Sep | 134mm | 2,852.0 | 2,855.0 | 3.0 | 3.0 | 100% |
| 14-Sep | 134mm | 2,855.0 | 2,861.0 | 6.0 | 6.0 | 100% |
| 14-Sep | 134mm | 2,861.0 | 2,865.0 | 4.0 | 1.5 | 38% |
| 15-Sep | 134mm | 2,865.0 | 2,866.0 | 1.0 | 0.0 | 0% |
| 15-Sep | 134mm | 2,866.0 | 2,868.0 | 2.0 | 0.0 | 0% |
| 16-Sep | 134mm | 2,868.0 | 2,871.0 | 3.0 | 0.0 | 0% |
| 16-Sep | 134mm | 2,871.0 | 2,874.0 | 3.0 | 0.0 | 0% |
| 16-Sep | 134mm | 2,874.0 | 2,877.0 | 3.0 | 0.0 | 0% |
| 16-Sep | 134mm | 2,877.0 | 2,889.0 | 12.0 | 5.0 | 42% |
| 16-Sep | 134mm | 2,889.0 | 2,892.0 | 3.0 | 2.5 | 83% |
| 16-Sep | 134mm | 2,892.0 | 2,894.0 | 2.0 | 2.0 | 100% |
| 16-Sep | 134mm | 2,894.0 | 2,896.0 | 2.0 | 1.0 | 50% |
| 17-Sep | 134mm | 2,896.0 | 2,901.0 | 5.0 | 5.0 | 100% |
| 17-Sep | 134mm | 2,901.0 | 2,910.0 | 9.0 | 9.0 | 100% |
| 17-Sep | 134mm | 2,910.0 | 2,914.0 | 4.0 | 4.0 | 100% |
| 17-Sep | 134mm | 2,914.0 | 2,918.0 | 4.0 | 4.0 | 100% |
| 17-Sep | 134mm | 2,918.0 | 2,922.0 | 4.0 | 4.0 | 100% |
| 17-Sep | 134mm | 2,922.0 | 2,926.0 | 4.0 | 3.0 | 75% |
| 17-Sep | 134mm | 2,926.0 | 2,927.0 | 1.0 | 0.0 | 0% |
| 17-Sep | 134mm | 2,927.0 | 2,928.5 | 1.5 | 0.5 | 33% |
| 17-Sep | 134mm | 2,928.5 | 2,930.0 | 1.5 | 0.5 | 33% |
| 17-Sep | 134mm | 2,930.0 | 2,933.0 | 3.0 | 3.0 | 100% |
| 17-Sep | 134mm | 2,933.0 | 2,935.5 | 2.5 | 0.0 | 0% |
| 18-Sep | 134mm | 2,935.5 | 2,938.0 | 2.5 | 0.5 | 20% |
| 18-Sep | 134mm | 2,938.0 | 2,944.0 | 6.0 | 6.0 | 100% |
| 18-Sep | 134mm | 2,944.0 | 2,946.0 | 2.0 | 0.0 | 0% |
| 18-Sep | 134mm | 2,946.0 | 2,947.0 | 1.0 | 1.0 | 100% |
| 18-Sep | 134mm | 2,947.0 | 2,949.0 | 2.0 | 0.0 | 0% |
| 18-Sep | 134mm | 2,949.0 | 2,950.0 | 1.0 | 0.5 | 50% |
| 18-Sep | 134mm | 2,950.0 | 2,951.5 | 1.5 | 1.5 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 18-Sep | 134mm | 2,951.5 | 2,952.0 | 0.5 | 0.0 | 0% |
| 18-Sep | 134mm | 2,952.0 | 2,954.5 | 2.5 | 0.5 | 20% |
| 18-Sep | 134mm | 2,954.5 | 2,957.0 | 2.5 | 2.5 | 100% |
| 19-Sep | 134mm | 2,957.0 | 2,961.0 | 4.0 | 4.0 | 100% |
| 19-Sep | 134mm | 2,961.0 | 2,967.0 | 6.0 | 6.0 | 100% |
| 19-Sep | 134mm | 2,967.0 | 2,973.0 | 6.0 | 6.0 | 100% |
| 19-Sep | 134mm | 2,973.0 | 2,977.0 | 4.0 | 4.0 | 100% |
| 19-Sep | 134mm | 2,977.0 | 2,983.0 | 6.0 | 6.0 | 100% |
| 19-Sep | 134mm | 2,983.0 | 2,986.0 | 3.0 | 3.0 | 100% |
| 19-Sep | 134mm | 2,986.0 | 2,989.0 | 3.0 | 3.0 | 100% |
| 19-Sep | 134mm | 2,989.0 | 2,993.0 | 4.0 | 4.0 | 100% |
| 20-Sep | 134mm | 2,993.0 | 2,997.0 | 4.0 | 4.0 | 100% |
| 20-Sep | 134mm | 2,997.0 | 3,003.0 | 6.0 | 6.0 | 100% |
| 20-Sep | 134mm | 3,003.0 | 3,008.0 | 5.0 | 5.0 | 100% |
| 20-Sep | 134mm | 3,008.0 | 3,020.0 | 12.0 | 12.0 | 100% |
| 20-Sep | 134mm | 3,020.0 | 3,021.0 | 1.0 | 0.0 | 0% |
| 22-Sep | 134mm | 3,021.0 | 3,027.0 | 6.0 | 6.0 | 100% |
| 22-Sep | 134mm | 3,027.0 | 3,037.0 | 10.0 | 10.0 | 100% |
| 23-Sep | 134mm | 3,037.0 | 3,047.5 | 10.5 | 10.5 | 100% |
| 23-Sep | 134mm | 3,047.5 | 3,058.0 | 10.5 | 10.5 | 100% |
| 23-Sep | 134mm | 3,058.0 | 3,068.0 | 10.0 | 10.0 | 100% |
| 23-Sep | 134mm | 3,068.0 | 3,078.0 | 10.0 | 10.0 | 100% |
| 23-Sep | 134mm | 3,078.0 | 3,088.0 | 10.0 | 10.0 | 100% |
| 23-Sep | 134mm | 3,088.0 | 3,098.0 | 10.0 | 10.0 | 100% |
| 23-Sep | 134mm | 3,098.0 | 3,104.0 | 6.0 | 6.0 | 100% |
| 24-Sep | 134mm | 3,104.0 | 3,113.0 | 9.0 | 9.0 | 100% |
| 24-Sep | 134mm | 3,113.0 | 3,121.0 | 8.0 | 10.0 | 125% |
| 24-Sep | 134mm | 3,121.0 | 3,133.0 | 12.0 | 10.0 | 83% |
| 24-Sep | 134mm | 3,133.0 | 3,143.0 | 10.0 | 10.0 | 100% |
| 24-Sep | 134mm | 3,143.0 | 3,152.0 | 9.0 | 9.0 | 100% |
| 24-Sep | 134mm | 3,152.0 | 3,162.0 | 10.0 | 10.0 | 100% |
| 24-Sep | 134mm | 3,162.0 | 3,172.0 | 10.0 | 10.0 | 100% |
| 25-Sep | 134mm | 3,172.0 | 3,182.0 | 10.0 | 10.0 | 100% |
| 25-Sep | 134mm | 3,182.0 | 3,192.0 | 10.0 | 10.0 | 100% |
| 25-Sep | 134mm | 3,192.0 | 3,202.0 | 10.0 | 10.0 | 100% |
| 25-Sep | 134mm | 3,202.0 | 3,207.0 | 5.0 | 5.0 | 100% |
| 25-Sep | 134mm | 3,207.0 | 3,211.0 | 4.0 | 4.0 | 100% |
| 25-Sep | 134mm | 3,211.0 | 3,221.0 | 10.0 | 10.0 | 100% |
| 25-Sep | 134mm | 3,221.0 | 3,231.0 | 10.0 | 10.0 | 100% |
| 26-Sep | HQ | 3,231.0 | 3,237.0 | 6.0 | 6.0 | 100% |
| 26-Sep | HQ | 3,237.0 | 3,241.0 | 4.0 | 4.0 | 100% |
| 26-Sep | HQ | 3,241.0 | 3,246.0 | 5.0 | 5.0 | 100% |
| 26-Sep | HQ | 3,246.0 | 3,251.0 | 5.0 | 5.0 | 100% |
| 26-Sep | HQ | 3,251.0 | 3,257.0 | 6.0 | 6.0 | 100% |
| 26-Sep | HQ | 3,257.0 | 3,261.0 | 4.0 | 4.0 | 100% |
| 26-Sep | HQ | 3,261.0 | 3,266.0 | 5.0 | 5.0 | 100% |
| 27-Sep | HQ | 3,266.0 | 3,275.0 | 9.0 | 9.0 | 100% |
| 27-Sep | HQ | 3,275.0 | 3,285.0 | 10.0 | 10.0 | 100% |
| 27-Sep | HQ | 3,285.0 | 3,295.0 | 10.0 | 10.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 27-Sep | HQ | 3,295.0 | 3,298.0 | 3.0 | 1.0 | 33% |
| 27-Sep | HQ | 3,298.0 | 3,303.0 | 5.0 | 3.0 | 60% |
| 27-Sep | HQ | 3,303.0 | 3,305.0 | 2.0 | 0.0 | 0% |
| 27-Sep | HQ | 3,305.0 | 3,305.5 | 0.5 | 0.0 | 0% |
| 27-Sep | HQ | 3,305.5 | 3,308.0 | 2.5 | 0.0 | 0% |
| 28-Sep | HQ | 3,308.0 | 3,314.0 | 6.0 | 1.0 | 17% |
| 28-Sep | HQ | 3,314.0 | 3,318.0 | 4.0 | 0.0 | 0% |
| 28-Sep | HQ | 3,318.0 | 3,320.0 | 2.0 | 0.5 | 25% |
| 28-Sep | HQ | 3,320.0 | 3,323.5 | 3.5 | 0.0 | 0% |
| 28-Sep | HQ | 3,323.5 | 3,325.0 | 1.5 | 0.5 | 33% |
| 28-Sep | HQ | 3,325.0 | 3,327.0 | 2.0 | 2.0 | 100% |
| 28-Sep | HQ | 3,327.0 | 3,329.0 | 2.0 | 2.0 | 100% |
| 29-Sep | HQ | 3,329.0 | 3,332.0 | 3.0 | 0.0 | 0% |
| 29-Sep | HQ | 3,332.0 | 3,336.0 | 4.0 | 0.5 | 13% |
| 29-Sep | HQ | 3,336.0 | 3,337.0 | 1.0 | 0.5 | 50% |
| 29-Sep | HQ | 3,337.0 | 3,339.0 | 2.0 | 2.0 | 100% |
| 29-Sep | HQ | 3,339.0 | 3,343.0 | 4.0 | 4.0 | 100% |
| 29-Sep | HQ | 3,343.0 | 3,346.0 | 3.0 | 3.0 | 100% |
| 30-Sep | HQ | 3,346.0 | 3,352.0 | 6.0 | 6.0 | 100% |
| 30-Sep | HQ | 3,352.0 | 3,356.0 | 4.0 | 4.0 | 100% |
| 30-Sep | HQ | 3,356.0 | 3,364.0 | 8.0 | 8.0 | 100% |
| 30-Sep | HQ | 3,364.0 | 3,368.0 | 4.0 | 3.0 | 75% |
| 30-Sep | HQ | 3,368.0 | 3,372.0 | 4.0 | 4.0 | 100% |
| 30-Sep | HQ | 3,372.0 | 3,377.0 | 5.0 | 5.0 | 100% |
| 01-Oct | HQ | 3,377.0 | 3,385.0 | 8.0 | 8.0 | 100% |
| 01-Oct | HQ | 3,385.0 | 3,389.0 | 4.0 | 1.5 | 38% |
| 01-Oct | HQ | 3,389.0 | 3,393.0 | 4.0 | 2.0 | 50% |
| 01-Oct | HQ | 3,393.0 | 3,396.0 | 3.0 | 1.0 | 33% |
| 01-Oct | HQ | 3,396.0 | 3,397.5 | 1.5 | 1.0 | 67% |
| 01-Oct | HQ | 3,397.5 | 3,399.0 | 1.5 | 1.5 | 100% |
| 01-Oct | HQ | 3,399.0 | 3,402.0 | 3.0 | 3.0 | 100% |
| 02-Oct | HQ | 3,402.0 | 3,405.0 | 3.0 | 2.0 | 67% |
| 02-Oct | HQ | 3,405.0 | 3,408.0 | 3.0 | 3.0 | 100% |
| 02-Oct | HQ | 3,408.0 | 3,411.0 | 3.0 | 1.0 | 33% |
| 02-Oct | HQ | 3,411.0 | 3,414.0 | 3.0 | 0.2 | 7% |
| 02-Oct | HQ | 3,414.0 | 3,415.5 | 1.5 | 1.0 | 67% |
| 02-Oct | HQ | 3,415.5 | 3,417.0 | 1.5 | 1.5 | 100% |
| 02-Oct | HQ | 3,417.0 | 3,422.0 | 5.0 | 5.0 | 100% |
| 03-Oct | HQ | 3,422.0 | 3,429.0 | 7.0 | 7.0 | 100% |
| 03-Oct | HQ | 3,429.0 | 3,438.0 | 9.0 | 9.0 | 100% |
| 03-Oct | HQ | 3,438.0 | 3,447.0 | 9.0 | 9.0 | 100% |
| 03-Oct | HQ | 3,447.0 | 3,453.0 | 6.0 | 6.0 | 100% |
| 03-Oct | HQ | 3,453.0 | 3,462.0 | 9.0 | 9.0 | 100% |
| 04-Oct | HQ | 3,462.0 | 3,472.0 | 10.0 | 10.0 | 100% |
| 04-Oct | HQ | 3,472.0 | 3,482.0 | 10.0 | 6.0 | 60% |
| 04-Oct | HQ | 3,482.0 | 3,491.0 | 9.0 | 9.0 | 100% |
| 04-Oct | HQ | 3,491.0 | 3,498.0 | 7.0 | 7.0 | 100% |
| 05-Oct | HQ | 3,498.0 | 3,508.0 | 10.0 | 10.0 | 100% |
| 05-Oct | HQ | 3,508.0 | 3,510.0 | 2.0 | 0.0 | 0% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 05-Oct | HQ | 3,510.0 | 3,512.0 | 2.0 | 1.0 | 50% |
| 05-Oct | HQ | 3,512.0 | 3,512.5 | 0.5 | 0.0 | 0% |
| 06-Oct | HQ | 3,512.5 | 3,513.0 | 0.5 | 0.1 | 20% |
| 06-Oct | HQ | 3,513.0 | 3,523.0 | 10.0 | 7.0 | 70% |
| 06-Oct | HQ | 3,523.0 | 3,527.0 | 4.0 | 0.0 | 0% |
| 06-Oct | HQ | 3,529.0 | 3,532.0 | 3.0 | 0.0 | 0% |
| 06-Oct | HQ | 3,532.0 | 3,538.0 | 6.0 | 0.0 | 0% |
| 07-Oct | HQ | 3,538.0 | 3,540.5 | 2.5 | 0.3 | 12% |
| 07-Oct | HQ | 3,540.5 | 3,541.0 | 0.5 | 0.0 | 0% |
| 07-Oct | HQ | 3,541.0 | 3,545.0 | 4.0 | 0.0 | 0% |
| 07-Oct | HQ | 3,545.0 | 3,548.0 | 3.0 | 0.0 | 0% |
| 07-Oct | HQ | 3,548.0 | 3,549.0 | 1.0 | 0.0 | 0% |
| 07-Oct | HQ | 3,549.0 | 3,550.0 | 1.0 | 0.0 | 0% |
| 08-Oct | HQ | 3,550.0 | 3,550.5 | 0.5 | 0.0 | 0% |
| 08-Oct | HQ | 3,550.5 | 3,559.0 | 8.5 | 1.0 | 12% |
| 08-Oct | HQ | 3,559.0 | 3,564.0 | 5.0 | 3.0 | 60% |
| 08-Oct | HQ | 3,564.0 | 3,564.5 | 0.5 | 0.0 | 0% |
| 09-Oct | HQ | 3,564.0 | 3,570.0 | 6.0 | 6.0 | 100% |
| 09-Oct | HQ | 3,570.0 | 3,574.0 | 4.0 | 4.0 | 100% |
| 09-Oct | HQ | 3,574.0 | 3,576.0 | 2.0 | 2.0 | 100% |
| 09-Oct | HQ | 3,576.0 | 3,580.0 | 4.0 | 4.0 | 100% |
| 09-Oct | HQ | 3,580.0 | 3,590.0 | 10.0 | 4.0 | 40% |
| 10-Oct | HQ | 3,590.0 | 3,600.0 | 10.0 | 10.0 | 100% |
| 10-Oct | HQ | 3,600.0 | 3,608.0 | 8.0 | 8.0 | 100% |
| 10-Oct | HQ | 3,608.0 | 3,610.0 | 2.0 | 1.0 | 50% |
| 10-Oct | HQ | 3,610.0 | 3,618.0 | 8.0 | 8.0 | 100% |
| 10-Oct | HQ | 3,618.0 | 3,621.0 | 3.0 | 3.0 | 100% |
| 10-Oct | HQ | 3,621.0 | 3,625.0 | 4.0 | 2.0 | 50% |
| 11-Oct | HQ | 3,625.0 | 3,630.0 | 5.0 | 2.0 | 40% |
| 11-Oct | HQ | 3,630.0 | 3,633.0 | 3.0 | 3.0 | 100% |
| 11-Oct | HQ | 3,633.0 | 3,637.0 | 4.0 | 4.0 | 100% |
| 11-Oct | HQ | 3,637.0 | 3,646.0 | 9.0 | 9.0 | 100% |
| 11-Oct | HQ | 3,646.0 | 3,650.0 | 4.0 | 2.0 | 50% |
| 11-Oct | HQ | 3,650.0 | 3,660.0 | 10.0 | 10.0 | 100% |
| 12-Oct | HQ | 3,660.0 | 3,670.0 | 10.0 | 10.0 | 100% |
| 12-Oct | HQ | 3,670.0 | 3,680.0 | 10.0 | 10.0 | 100% |
| 12-Oct | HQ | 3,680.0 | 3,690.0 | 10.0 | 10.0 | 100% |
| 12-Oct | HQ | 3,690.0 | 3,700.0 | 10.0 | 10.0 | 100% |
| 12-Oct | HQ | 3,700.0 | 3,706.0 | 6.0 | 6.0 | 100% |
| 12-Oct | HQ | 3,706.0 | 3,716.0 | 10.0 | 10.0 | 100% |
| 13-Oct | HQ | 3,716.0 | 3,726.0 | 10.0 | 10.0 | 100% |
| 13-Oct | HQ | 3,726.0 | 3,732.0 | 6.0 | 6.0 | 100% |
| 13-Oct | HQ | 3,732.0 | 3,740.0 | 8.0 | 8.0 | 100% |
| 13-Oct | HQ | 3,740.0 | 3,749.0 | 9.0 | 4.5 | 50% |
| 13-Oct | HQ | 3,749.0 | 3,755.0 | 6.0 | 6.0 | 100% |
| 13-Oct | HQ | 3,755.0 | 3,765.0 | 10.0 | 10.0 | 100% |
| 13-Oct | HQ | 3,765.0 | 3,775.0 | 10.0 | 10.0 | 100% |
| 14-Oct | HQ | 3,775.0 | 3,785.0 | 10.0 | 10.0 | 100% |
| 14-Oct | HQ | 3,785.0 | 3,795.0 | 10.0 | 10.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 14-Oct | HQ | 3,795.0 | 3,805.0 | 10.0 | 10.0 | 100% |
| 14-Oct | HQ | 3,805.0 | 3,814.0 | 9.0 | 9.0 | 100% |
| 14-Oct | HQ | 3,814.0 | 3,824.0 | 10.0 | 10.0 | 100% |
| 14-Oct | HQ | 3,824.0 | 3,834.0 | 10.0 | 10.0 | 100% |
| 14-Oct | HQ | 3,834.0 | 3,844.0 | 10.0 | 10.0 | 100% |
| 15-Oct | HQ | 3,844.0 | 3,849.0 | 5.0 | 5.0 | 100% |
| 15-Oct | HQ | 3,849.0 | 3,853.0 | 4.0 | 4.0 | 100% |
| 15-Oct | HQ | 3,853.0 | 3,855.0 | 2.0 | 1.0 | 50% |
| 15-Oct | HQ | 3,855.0 | 3,858.0 | 3.0 | 3.0 | 100% |
| 15-Oct | HQ | 3,858.0 | 3,862.0 | 4.0 | 4.0 | 100% |
| 15-Oct | HQ | 3,862.0 | 3,863.0 | 1.0 | 1.0 | 100% |
| 15-Oct | HQ | 3,863.0 | 3,865.5 | 2.5 | 0.5 | 20% |
| 15-Oct | HQ | 3,865.5 | 3,867.0 | 1.5 | 1.5 | 100% |
| 15-Oct | HQ | 3,867.0 | 3,870.0 | 3.0 | 2.0 | 67% |
| 16-Oct | HQ | 3,870.0 | 3,872.0 | 2.0 | 0.0 | 0% |
| 16-Oct | HQ | 3,872.0 | 3,874.0 | 2.0 | 2.0 | 100% |
| 16-Oct | HQ | 3,874.0 | 3,876.0 | 2.0 | 2.0 | 100% |
| 16-Oct | HQ | 3,876.0 | 3,884.0 | 8.0 | 7.5 | 94% |
| 16-Oct | HQ | 3,884.0 | 3,885.0 | 1.0 | 0.0 | 0% |
| 16-Oct | HQ | 3,885.0 | 3,887.5 | 2.5 | 2.5 | 100% |
| 16-Oct | HQ | 3,887.5 | 3,892.0 | 4.5 | 4.0 | 89% |
| 17-Oct | HQ | 3,892.0 | 3,895.0 | 3.0 | 3.0 | 100% |
| 17-Oct | HQ | 3,895.0 | 3,897.0 | 2.0 | 2.0 | 100% |
| 17-Oct | HQ | 3,897.0 | 3,904.0 | 7.0 | 7.0 | 100% |
| 17-Oct | HQ | 3,904.0 | 3,906.0 | 2.0 | 2.0 | 100% |
| 17-Oct | HQ | 3,906.0 | 3,908.0 | 2.0 | 2.0 | 100% |
| 17-Oct | HQ | 3,908.0 | 3,911.0 | 3.0 | 3.0 | 100% |
| 17-Oct | HQ | 3,911.0 | 3,918.5 | 7.5 | 7.5 | 100% |
| 17-Oct | HQ | 3,918.5 | 3,920.0 | 1.5 | 1.5 | 100% |
| 18-Oct | HQ | 3,920.0 | 3,920.5 | 0.5 | 0.5 | 100% |
| 18-Oct | HQ | 3,920.5 | 3,922.0 | 1.5 | 0.0 | 0% |
| 18-Oct | HQ | 3,922.0 | 3,924.0 | 2.0 | 2.0 | 100% |
| 18-Oct | HQ | 3,924.0 | 3,926.0 | 2.0 | 2.0 | 100% |
| 18-Oct | HQ | 3,926.0 | 3,934.0 | 8.0 | 8.0 | 100% |
| 19-Oct | HQ | 3,934.0 | 3,939.0 | 5.0 | 4.5 | 90% |
| 19-Oct | HQ | 3,939.0 | 3,944.0 | 5.0 | 5.0 | 100% |
| 19-Oct | HQ | 3,944.0 | 3,949.0 | 5.0 | 5.0 | 100% |
| 19-Oct | HQ | 3,949.0 | 3,951.0 | 2.0 | 2.0 | 100% |
| 19-Oct | HQ | 3,951.0 | 3,956.0 | 5.0 | 5.0 | 100% |
| 19-Oct | HQ | 3,956.0 | 3,966.0 | 10.0 | 10.0 | 100% |
| 19-Oct | HQ | 3,966.0 | 3,968.0 | 2.0 | 2.0 | 100% |
| 19-Oct | HQ | 3,968.0 | 3,971.0 | 3.0 | 3.0 | 100% |
| 19-Oct | HQ | 3,971.0 | 3,976.0 | 5.0 | 5.0 | 100% |
| 20-Oct | HQ | 3,976.0 | 3,981.0 | 5.0 | 5.0 | 100% |
| 20-Oct | HQ | 3,981.0 | 3,986.0 | 5.0 | 5.0 | 100% |
| 20-Oct | HQ | 3,986.0 | 3,991.0 | 5.0 | 5.0 | 100% |
| 21-Oct | HQ | 3,991.0 | 3,996.0 | 5.0 | 4.0 | 80% |
| 21-Oct | HQ | 3,996.0 | 4,003.0 | 7.0 | 7.0 | 100% |
| 21-Oct | HQ | 4,003.0 | 4,005.0 | 2.0 | 2.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 21-Oct | HQ | 4,005.0 | 4,010.0 | 5.0 | 5.0 | 100% |
| 21-Oct | HQ | 4,010.0 | 4,012.0 | 2.0 | 2.0 | 100% |
| 21-Oct | HQ | 4,012.0 | 4,015.0 | 3.0 | 3.0 | 100% |
| 21-Oct | HQ | 4,015.0 | 4,020.0 | 5.0 | 4.0 | 80% |
| 21-Oct | HQ | 4,020.0 | 4,023.0 | 3.0 | 0.0 | 0% |
| 21-Oct | HQ | 4,023.0 | 4,025.0 | 2.0 | 1.0 | 50% |
| 21-Oct | HQ | 4,025.0 | 4,026.0 | 1.0 | 0.0 | 0% |
| 22-Oct | HQ | 4,026.0 | 4,028.0 | 2.0 | 2.0 | 100% |
| 22-Oct | HQ | 4,028.0 | 4,028.5 | 0.5 | 0.5 | 100% |
| 22-Oct | HQ | 4,028.5 | 4,030.0 | 1.5 | 1.0 | 67% |
| 22-Oct | HQ | 4,030.0 | 4,033.0 | 3.0 | 3.0 | 100% |
| 22-Oct | HQ | 4,033.0 | 4,034.0 | 1.0 | 1.0 | 100% |
| 22-Oct | HQ | 4,034.0 | 4,037.0 | 3.0 | 2.0 | 67% |
| 23-Oct | HQ | 4,037.0 | 4,043.0 | 6.0 | 6.0 | 100% |
| 23-Oct | HQ | 4,043.0 | 4,046.0 | 3.0 | 3.0 | 100% |
| 23-Oct | HQ | 4,046.0 | 4,050.0 | 4.0 | 3.0 | 75% |
| 23-Oct | HQ | 4,050.0 | 4,052.0 | 2.0 | 2.0 | 100% |
| 23-Oct | HQ | 4,052.0 | 4,053.0 | 1.0 | 1.0 | 100% |
| 23-Oct | HQ | 4,053.0 | 4,056.5 | 3.5 | 3.5 | 100% |
| 23-Oct | HQ | 4,056.5 | 4,061.0 | 4.5 | 3.0 | 67% |
| 23-Oct | HQ | 4,061.0 | 4,062.5 | 1.5 | 0.5 | 33% |
| 23-Oct | HQ | 4,062.5 | 4,063.5 | 1.0 | 1.0 | 100% |
| 23-Oct | HQ | 4,063.5 | 4,064.0 | 0.5 | 0.0 | 0% |
| 24-Oct | HQ | 4,064.0 | 4,064.5 | 0.5 | 0.5 | 100% |
| 24-Oct | HQ | 4,064.5 | 4,065.5 | 1.0 | 1.0 | 100% |
| 24-Oct | HQ | 4,065.5 | 4,069.0 | 3.5 | 2.0 | 57% |
| 24-Oct | HQ | 4,069.0 | 4,071.0 | 2.0 | 1.0 | 50% |
| 24-Oct | HQ | 4,071.0 | 4,072.5 | 1.5 | 0.0 | 0% |
| 24-Oct | HQ | 4,072.5 | 4,074.0 | 1.5 | 1.5 | 100% |
| 24-Oct | HQ | 4,074.0 | 4,074.5 | 0.5 | 0.5 | 100% |
| 24-Oct | HQ | 4,074.5 | 4,078.5 | 4.0 | 4.0 | 100% |
| 24-Oct | HQ | 4,078.5 | 4,081.5 | 3.0 | 3.0 | 100% |
| 25-Oct | HQ | 4,081.5 | 4,085.0 | 3.5 | 3.5 | 100% |
| 25-Oct | HQ | 4,085.0 | 4,087.0 | 2.0 | 2.0 | 100% |
| 25-Oct | HQ | 4,087.0 | 4,088.5 | 1.5 | 1.0 | 67% |
| 25-Oct | HQ | 4,088.5 | 4,091.0 | 2.5 | 2.5 | 100% |
| 25-Oct | HQ | 4,091.0 | 4,093.0 | 2.0 | 2.0 | 100% |
| 25-Oct | HQ | 4,093.0 | 4,094.0 | 1.0 | 0.5 | 50% |
| 25-Oct | HQ | 4,094.0 | 4,097.0 | 3.0 | 3.0 | 100% |
| 25-Oct | HQ | 4,097.0 | 4,098.0 | 1.0 | 0.5 | 50% |
| 26-Oct | HQ | 4,098.0 | 4,100.0 | 2.0 | 2.0 | 100% |
| 26-Oct | HQ | 4,100.0 | 4,105.0 | 5.0 | 4.0 | 80% |
| 26-Oct | HQ | 4,105.0 | 4,106.0 | 1.0 | 0.5 | 50% |
| 26-Oct | HQ | 4,106.0 | 4,106.1 | 0.1 | 0.1 | 100% |
| 26-Oct | HQ | 4,106.1 | 4,108.5 | 2.4 | 2.0 | 83% |
| 26-Oct | HQ | 4,108.5 | 4,110.0 | 1.5 | 0.5 | 33% |
| 26-Oct | HQ | 4,110.0 | 4,111.5 | 1.5 | 1.0 | 67% |
| 26-Oct | HQ | 4,111.5 | 4,113.0 | 1.5 | 1.5 | 100% |
| 27-Oct | HQ | 4,113.0 | 4,115.0 | 2.0 | 0.5 | 25% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 27-Oct | HQ | 4,115.0 | 4,116.0 | 1.0 | 0.5 | 50% |
| 27-Oct | HQ | 4,116.0 | 4,119.0 | 3.0 | 3.0 | 100% |
| 27-Oct | HQ | 4,119.0 | 4,119.5 | 0.5 | 0.5 | 100% |
| 27-Oct | HQ | 4,119.5 | 4,120.5 | 1.0 | 0.2 | 20% |
| 28-Oct | HQ | 4,120.5 | 4,130.0 | 9.5 | 9.5 | 100% |
| 28-Oct | HQ | 4,130.0 | 4,132.5 | 2.5 | 2.5 | 100% |
| 28-Oct | HQ | 4,132.5 | 4,134.5 | 2.0 | 1.5 | 75% |
| 28-Oct | HQ | 4,134.5 | 4,135.0 | 0.5 | 0.5 | 100% |
| 29-Oct | HQ | 4,135.0 | 4,140.5 | 5.5 | 5.5 | 100% |
| 29-Oct | HQ | 4,140.5 | 4,145.0 | 4.5 | 3.5 | 78% |
| 29-Oct | HQ | 4,145.0 | 4,151.0 | 6.0 | 5.5 | 92% |
| 29-Oct | HQ | 4,151.0 | 4,156.0 | 5.0 | 5.0 | 100% |
| 29-Oct | HQ | 4,156.0 | 4,162.0 | 6.0 | 3.5 | 58% |
| 29-Oct | HQ | 4,162.0 | 4,166.0 | 4.0 | 3.0 | 75% |
| 29-Oct | HQ | 4,166.0 | 4,167.0 | 1.0 | 0.0 | 0% |
| 30-Oct | HQ | 4,167.0 | 4,168.5 | 1.5 | 0.5 | 33% |
| 30-Oct | HQ | 4,168.5 | 4,173.0 | 4.5 | 3.0 | 67% |
| 30-Oct | HQ | 4,173.0 | 4,176.0 | 3.0 | 1.0 | 33% |
| 30-Oct | HQ | 4,176.0 | 4,180.0 | 4.0 | 1.0 | 25% |
| 30-Oct | HQ | 4,180.0 | 4,181.0 | 1.0 | 1.0 | 100% |
| 30-Oct | HQ | 4,181.0 | 4,181.5 | 0.5 | 0.5 | 100% |
| 31-Oct | HQ | 4,181.5 | 4,182.0 | 0.5 | 0.5 | 100% |
| 31-Oct | HQ | 4,182.0 | 4,184.0 | 2.0 | 2.0 | 100% |
| 31-Oct | HQ | 4,184.0 | 4,186.0 | 2.0 | 1.0 | 50% |
| 31-Oct | HQ | 4,186.0 | 4,188.0 | 2.0 | 1.5 | 75% |
| 01-Nov | HQ | 4,188.0 | 4,196.5 | 8.5 | 2.5 | 29% |
| 01-Nov | HQ | 4,196.5 | 4,198.5 | 2.0 | 2.0 | 100% |
| 01-Nov | HQ | 4,198.5 | 4,200.5 | 2.0 | 1.5 | 75% |
| 01-Nov | HQ | 4,200.5 | 4,202.0 | 1.5 | 1.5 | 100% |
| 01-Nov | HQ | 4,202.0 | 4,205.0 | 3.0 | 3.0 | 100% |
| 01-Nov | HQ | 4,205.0 | 4,209.0 | 4.0 | 2.5 | 63% |
| 01-Nov | HQ | 4,209.0 | 4,211.0 | 2.0 | 1.5 | 75% |
| 01-Nov | HQ | 4,211.0 | 4,214.0 | 3.0 | 1.5 | 50% |
| 02-Nov | HQ | 4,214.0 | 4,218.5 | 4.5 | 2.0 | 44% |
| 02-Nov | HQ | 4,218.5 | 4,222.5 | 4.0 | 1.0 | 25% |
| 02-Nov | HQ | 4,222.5 | 4,223.5 | 1.0 | 1.0 | 100% |
| 02-Nov | HQ | 4,223.5 | 4,226.0 | 2.5 | 1.0 | 40% |
| 03-Nov | HQ | 4,226.0 | 4,231.0 | 5.0 | 4.0 | 80% |
| 03-Nov | HQ | 4,231.0 | 4,234.0 | 3.0 | 3.0 | 100% |
| 03-Nov | HQ | 4,234.0 | 4,236.0 | 2.0 | 1.5 | 75% |
| 03-Nov | HQ | 4,236.0 | 4,236.5 | 0.5 | 0.0 | 0% |
| 04-Nov | HQ | 4,236.5 | 4,239.5 | 3.0 | 2.5 | 83% |
| 04-Nov | HQ | 4,239.5 | 4,242.0 | 2.5 | 2.0 | 80% |
| 04-Nov | HQ | 4,242.0 | 4,244.0 | 2.0 | 1.0 | 50% |
| 04-Nov | HQ | 4,244.0 | 4,248.0 | 4.0 | 2.0 | 50% |
| 05-Nov | HQ | 4,248.0 | 4,253.0 | 5.0 | 0.5 | 10% |
| 05-Nov | HQ | 4,253.0 | 4,255.0 | 2.0 | 2.0 | 100% |
| 05-Nov | HQ | 4,255.0 | 4,258.0 | 3.0 | 0.5 | 17% |
| 05-Nov | HQ | 4,258.0 | 4,259.5 | 1.5 | 1.5 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 05-Nov | HQ | 4,259.5 | 4,260.5 | 1.0 | 0.0 | 0% |
| 06-Nov | HQ | 4,260.5 | 4,261.0 | 0.5 | 0.0 | 0% |
| 06-Nov | HQ | 4,261.0 | 4,262.0 | 1.0 | 0.5 | 50% |
| 06-Nov | HQ | 4,262.0 | 4,270.0 | 8.0 | 5.0 | 63% |
| 06-Nov | HQ | 4,270.0 | 4,273.0 | 3.0 | 1.0 | 33% |
| 06-Nov | HQ | 4,273.0 | 4,274.0 | 1.0 | 1.0 | 100% |
| 06-Nov | HQ | 4,274.0 | 4,277.0 | 3.0 | 1.0 | 33% |
| 06-Nov | HQ | 4,277.0 | 4,280.0 | 3.0 | 2.0 | 67% |
| 06-Nov | HQ | 4,280.0 | 4,284.0 | 4.0 | 4.0 | 100% |
| 06-Nov | HQ | 4,284.0 | 4,287.0 | 3.0 | 1.5 | 50% |
| 07-Nov | HQ | 4,287.0 | 4,289.5 | 2.5 | 2.5 | 100% |
| 07-Nov | HQ | 4,289.5 | 4,299.0 | 9.5 | 9.5 | 100% |
| 07-Nov | HQ | 4,299.0 | 4,300.0 | 1.0 | 1.0 | 100% |
| 07-Nov | HQ | 4,300.0 | 4,302.0 | 2.0 | 0.5 | 25% |
| 08-Nov | HQ | 4,302.0 | 4,305.5 | 3.5 | 1.0 | 29% |
| 08-Nov | HQ | 4,305.5 | 4,306.5 | 1.0 | 0.5 | 50% |
| 08-Nov | HQ | 4,306.5 | 4,307.0 | 0.5 | 0.5 | 100% |
| 09-Nov | HQ | 4,307.0 | 4,311.0 | 4.0 | 3.0 | 75% |
| 09-Nov | HQ | 4,311.0 | 4,315.0 | 4.0 | 4.0 | 100% |
| 09-Nov | HQ | 4,315.0 | 4,318.0 | 3.0 | 0.0 | 0% |
| 09-Nov | HQ | 4,318.0 | 4,320.0 | 2.0 | 2.0 | 100% |
| 09-Nov | HQ | 4,320.0 | 4,323.0 | 3.0 | 1.0 | 33% |
| 09-Nov | HQ | 4,323.0 | 4,324.5 | 1.5 | 0.0 | 0% |
| 11-Nov | NQ | 4,324.5 | 4,326.5 | 2.0 | 1.0 | 50% |
| 11-Nov | NQ | 4,326.5 | 4,327.5 | 1.0 | 1.0 | 100% |
| 11-Nov | NQ | 4,327.5 | 4,331.5 | 4.0 | 2.0 | 50% |
| 11-Nov | NQ | 4,331.5 | 4,333.5 | 2.0 | 1.0 | 50% |
| 11-Nov | NQ | 4,333.5 | 4,335.0 | 1.5 | 0.0 | 0% |
| 12-Nov | NQ | 4,335.0 | 4,345.0 | 10.0 | 7.0 | 70% |
| 12-Nov | NQ | 4,345.0 | 4,349.0 | 4.0 | 1.0 | 25% |
| 12-Nov | NQ | 4,349.0 | 4,351.5 | 2.5 | 2.0 | 80% |
| 12-Nov | NQ | 4,351.5 | 4,355.0 | 3.5 | 2.0 | 57% |
| 12-Nov | NQ | 4,355.0 | 4,358.0 | 3.0 | 1.5 | 50% |
| 12-Nov | NQ | 4,358.0 | 4,360.0 | 2.0 | 0.5 | 25% |
| 13-Nov | NQ | 4,360.0 | 4,362.0 | 2.0 | 2.0 | 100% |
| 13-Nov | NQ | 4,362.0 | 4,363.5 | 1.5 | 0.0 | 0% |
| 13-Nov | NQ | 4,363.5 | 4,364.0 | 0.5 | 0.0 | 0% |
| 15-Nov | NQ | 4,364.0 | 4,369.0 | 5.0 | 1.0 | 20% |
| 15-Nov | NQ | 4,369.0 | 4,377.0 | 8.0 | 8.0 | 100% |
| 15-Nov | NQ | 4,377.0 | 4,387.0 | 10.0 | 10.0 | 100% |
| 16-Nov | NQ | 4,387.0 | 4,393.5 | 6.5 | 6.5 | 100% |
| 16-Nov | NQ | 4,393.5 | 4,404.0 | 10.5 | 10.5 | 100% |
| 16-Nov | NQ | 4,404.0 | 4,407.5 | 3.5 | 3.5 | 100% |
| 16-Nov | NQ | 4,407.5 | 4,410.5 | 3.0 | 2.0 | 67% |
| 16-Nov | NQ | 4,410.5 | 4,414.0 | 3.5 | 3.5 | 100% |
| 16-Nov | NQ | 4,414.0 | 4,417.0 | 3.0 | 3.0 | 100% |
| 16-Nov | NQ | 4,417.0 | 4,420.5 | 3.5 | 3.5 | 100% |
| 16-Nov | NQ | 4,420.5 | 4,422.0 | 1.5 | 1.0 | 67% |
| 16-Nov | NQ | 4,422.0 | 4,423.0 | 1.0 | 0.5 | 50% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 16-Nov | NQ | 4,423.0 | 4,425.0 | 2.0 | 1.5 | 75% |
| 16-Nov | NQ | 4,425.0 | 4,429.0 | 4.0 | 4.0 | 100% |
| 17-Nov | NQ | 4,429.0 | 4,433.0 | 4.0 | 4.0 | 100% |
| 17-Nov | NQ | 4,433.0 | 4,437.5 | 4.5 | 4.5 | 100% |
| 17-Nov | NQ | 4,437.5 | 4,442.5 | 5.0 | 5.0 | 100% |
| 17-Nov | NQ | 4,442.5 | 4,444.5 | 2.0 | 2.0 | 100% |
| 17-Nov | NQ | 4,444.5 | 4,446.0 | 1.5 | 0.5 | 33% |
| 17-Nov | NQ | 4,446.0 | 4,447.5 | 1.5 | 1.5 | 100% |
| 17-Nov | NQ | 4,447.5 | 4,450.0 | 2.5 | 2.5 | 100% |
| 17-Nov | NQ | 4,450.0 | 4,451.5 | 1.5 | 1.0 | 67% |
| 17-Nov | NQ | 4,451.5 | 4,455.5 | 4.0 | 4.0 | 100% |
| 17-Nov | NQ | 4,455.5 | 4,460.0 | 4.5 | 4.0 | 89% |
| 18-Nov | NQ | 4,460.0 | 4,464.5 | 4.5 | 4.5 | 100% |
| 18-Nov | NQ | 4,464.5 | 4,466.5 | 2.0 | 2.0 | 100% |
| 18-Nov | NQ | 4,466.5 | 4,470.0 | 3.5 | 3.5 | 100% |
| 18-Nov | NQ | 4,470.0 | 4,472.0 | 2.0 | 2.0 | 100% |
| 18-Nov | NQ | 4,472.0 | 4,473.0 | 1.0 | 0.0 | 0% |
| 18-Nov | NQ | 4,473.0 | 4,474.5 | 1.5 | 1.0 | 67% |
| 18-Nov | NQ | 4,474.5 | 4,479.5 | 5.0 | 5.0 | 100% |
| 18-Nov | NQ | 4,479.5 | 4,487.0 | 7.5 | 7.5 | 100% |
| 18-Nov | NQ | 4,487.0 | 4,490.0 | 3.0 | 3.0 | 100% |
| 19-Nov | NQ | 4,490.0 | 4,500.0 | 10.0 | 10.0 | 100% |
| 19-Nov | NQ | 4,500.0 | 4,510.0 | 10.0 | 10.0 | 100% |
| 19-Nov | NQ | 4,510.0 | 4,520.0 | 10.0 | 10.0 | 100% |
| 19-Nov | NQ | 4,520.0 | 4,523.0 | 3.0 | 3.0 | 100% |
| 19-Nov | NQ | 4,523.0 | 4,524.5 | 1.5 | 1.0 | 67% |
| 19-Nov | NQ | 4,524.5 | 4,530.0 | 5.5 | 5.5 | 100% |
| 20-Nov | NQ | 4,530.0 | 4,534.0 | 4.0 | 4.0 | 100% |
| 20-Nov | NQ | 4,534.0 | 4,542.0 | 8.0 | 8.0 | 100% |
| 20-Nov | NQ | 4,542.0 | 4,545.0 | 3.0 | 3.0 | 100% |
| 20-Nov | NQ | 4,545.0 | 4,549.5 | 4.5 | 4.5 | 100% |
| 20-Nov | NQ | 4,549.5 | 4,557.0 | 7.5 | 7.5 | 100% |
| 21-Nov | NQ | 4,557.0 | 4,565.0 | 8.0 | 8.0 | 100% |
| 21-Nov | NQ | 4,565.0 | 4,572.0 | 7.0 | 7.0 | 100% |
| 21-Nov | NQ | 4,572.0 | 4,575.5 | 3.5 | 3.5 | 100% |
| 21-Nov | NQ | 4,575.5 | 4,578.0 | 2.5 | 0.5 | 20% |
| 21-Nov | NQ | 4,578.0 | 4,580.0 | 2.0 | 0.5 | 25% |
| 21-Nov | NQ | 4,580.0 | 4,581.5 | 1.5 | 0.5 | 33% |
| 21-Nov | NQ | 4,581.5 | 4,583.0 | 1.5 | 1.5 | 100% |
| 21-Nov | NQ | 4,583.0 | 4,585.0 | 2.0 | 0.5 | 25% |
| 21-Nov | NQ | 4,585.0 | 4,587.0 | 2.0 | 2.0 | 100% |
| 21-Nov | NQ | 4,587.0 | 4,589.0 | 2.0 | 0.5 | 25% |
| 21-Nov | NQ | 4,589.0 | 4,595.0 | 6.0 | 6.0 | 100% |
| 22-Nov | NQ | 4,595.0 | 4,597.0 | 2.0 | 2.0 | 100% |
| 23-Nov | NQ | 4,597.0 | 4,597.5 | 0.5 | 0.0 | 0% |
| 23-Nov | NQ | 4,597.5 | 4,599.0 | 1.5 | 1.0 | 67% |
| 23-Nov | NQ | 4,599.0 | 4,600.5 | 1.5 | 0.5 | 33% |
| 23-Nov | NQ | 4,600.5 | 4,602.0 | 1.5 | 0.0 | 0% |
| 24-Nov | NQ | 4,602.0 | 4,603.0 | 1.0 | 0.5 | 50% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 24-Nov | NQ | 4,603.0 | 4,604.5 | 1.5 | 1.5 | 100% |
| 24-Nov | NQ | 4,604.5 | 4,605.0 | 0.5 | 0.0 | 0% |
| 24-Nov | NQ | 4,605.0 | 4,607.0 | 2.0 | 2.0 | 100% |
| 24-Nov | NQ | 4,607.0 | 4,609.0 | 2.0 | 2.0 | 100% |
| 24-Nov | NQ | 4,609.0 | 4,610.0 | 1.0 | 1.0 | 100% |
| 24-Nov | NQ | 4,610.0 | 4,612.0 | 2.0 | 2.0 | 100% |
| 24-Nov | NQ | 4,612.0 | 4,614.5 | 2.5 | 2.0 | 80% |
| 24-Nov | NQ | 4,614.5 | 4,621.0 | 6.5 | 6.5 | 100% |
| 25-Nov | NQ | 4,621.0 | 4,624.0 | 3.0 | 3.0 | 100% |
| 25-Nov | NQ | 4,624.0 | 4,632.0 | 8.0 | 8.0 | 100% |
| 25-Nov | NQ | 4,632.0 | 4,635.0 | 3.0 | 3.0 | 100% |
| 25-Nov | NQ | 4,635.0 | 4,639.5 | 4.5 | 4.5 | 100% |
| 25-Nov | NQ | 4,639.5 | 4,643.0 | 3.5 | 3.5 | 100% |
| 25-Nov | NQ | 4,643.0 | 4,644.0 | 1.0 | 1.0 | 100% |
| 25-Nov | NQ | 4,644.0 | 4,646.0 | 2.0 | 2.0 | 100% |
| 25-Nov | NQ | 4,646.0 | 4,647.5 | 1.5 | 1.5 | 100% |
| 25-Nov | NQ | 4,647.5 | 4,648.0 | 0.5 | 0.0 | 0% |
| 25-Nov | NQ | 4,648.0 | 4,649.0 | 1.0 | 0.3 | 30% |
| 25-Nov | NQ | 4,649.0 | 4,650.0 | 1.0 | 0.5 | 50% |
| 26-Nov | NQ | 4,650.0 | 4,651.0 | 1.0 | 0.5 | 50% |
| 26-Nov | NQ | 4,651.0 | 4,660.0 | 9.0 | 9.0 | 100% |
| 26-Nov | NQ | 4,660.0 | 4,661.5 | 1.5 | 0.5 | 33% |
| 26-Nov | NQ | 4,661.5 | 4,666.5 | 5.0 | 5.0 | 100% |
| 26-Nov | NQ | 4,666.5 | 4,667.5 | 1.0 | 0.0 | 0% |
| 26-Nov | NQ | 4,667.5 | 4,669.0 | 1.5 | 1.5 | 100% |
| 26-Nov | NQ | 4,669.0 | 4,675.0 | 6.0 | 6.0 | 100% |
| 26-Nov | NQ | 4,675.0 | 4,677.5 | 2.5 | 2.5 | 100% |
| 26-Nov | NQ | 4,677.5 | 4,680.5 | 3.0 | 3.0 | 100% |
| 26-Nov | NQ | 4,680.5 | 4,684.5 | 4.0 | 4.0 | 100% |
| 27-Nov | NQ | 4,684.5 | 4,689.0 | 4.5 | 4.5 | 100% |
| 27-Nov | NQ | 4,689.0 | 4,695.0 | 6.0 | 6.0 | 100% |
| 27-Nov | NQ | 4,695.0 | 4,698.5 | 3.5 | 3.5 | 100% |
| 29-Nov | NQ | 4,699.0 | 4,701.0 | 2.0 | 2.0 | 100% |
| 29-Nov | NQ | 4,701.0 | 4,704.0 | 3.0 | 2.5 | 83% |
| 29-Nov | NQ | 4,704.0 | 4,705.5 | 1.5 | 0.5 | 33% |
| 29-Nov | NQ | 4,705.5 | 4,707.5 | 2.0 | 2.0 | 100% |
| 29-Nov | NQ | 4,707.5 | 4,709.0 | 1.5 | 1.0 | 67% |
| 29-Nov | NQ | 4,709.0 | 4,710.5 | 1.5 | 1.0 | 67% |
| 29-Nov | NQ | 4,710.5 | 4,714.0 | 3.5 | 3.5 | 100% |
| 29-Nov | NQ | 4,714.0 | 4,719.0 | 5.0 | 5.0 | 100% |
| 29-Nov | NQ | 4,719.0 | 4,721.0 | 2.0 | 1.5 | 75% |
| 29-Nov | NQ | 4,721.0 | 4,723.5 | 2.5 | 2.5 | 100% |
| 30-Nov | NQ | 4,723.5 | 4,724.5 | 1.0 | 0.5 | 50% |
| 30-Nov | NQ | 4,724.5 | 4,727.5 | 3.0 | 3.0 | 100% |
| 30-Nov | NQ | 4,727.5 | 4,730.0 | 2.5 | 2.5 | 100% |
| 30-Nov | NQ | 4,730.0 | 4,733.5 | 3.5 | 2.0 | 57% |
| 30-Nov | NQ | 4,733.5 | 4,735.0 | 1.5 | 1.0 | 67% |
| 30-Nov | NQ | 4,735.0 | 4,736.0 | 1.0 | 0.5 | 50% |
| 30-Nov | NQ | 4,736.0 | 4,739.0 | 3.0 | 3.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 30-Nov | NQ | 4,739.0 | 4,744.0 | 5.0 | 5.0 | 100% |
| 30-Nov | NQ | 4,744.0 | 4,748.0 | 4.0 | 4.0 | 100% |
| 30-Nov | NQ | 4,748.0 | 4,753.0 | 5.0 | 5.0 | 100% |
| 01-Dec | NQ | 4,753.0 | 4,754.0 | 1.0 | 0.5 | 50% |
| 01-Dec | NQ | 4,754.0 | 4,755.5 | 1.5 | 0.5 | 33% |
| 01-Dec | NQ | 4,755.5 | 4,757.5 | 2.0 | 1.0 | 50% |
| 01-Dec | NQ | 4,757.5 | 4,760.0 | 2.5 | 2.5 | 100% |
| 01-Dec | NQ | 4,760.0 | 4,761.0 | 1.0 | 1.0 | 100% |
| 01-Dec | NQ | 4,761.0 | 4,762.0 | 1.0 | 0.0 | 0% |
| 01-Dec | NQ | 4,762.0 | 4,766.0 | 4.0 | 3.5 | 88% |
| 01-Dec | NQ | 4,766.0 | 4,771.0 | 5.0 | 5.0 | 100% |
| 01-Dec | NQ | 4,771.0 | 4,773.5 | 2.5 | 2.5 | 100% |
| 01-Dec | NQ | 4,773.5 | 4,777.5 | 4.0 | 4.0 | 100% |
| 02-Dec | NQ | 4,777.5 | 4,782.0 | 4.5 | 4.5 | 100% |
| 02-Dec | NQ | 4,782.0 | 4,786.0 | 4.0 | 4.0 | 100% |
| 02-Dec | NQ | 4,786.0 | 4,788.0 | 2.0 | 2.0 | 100% |
| 02-Dec | NQ | 4,788.0 | 4,790.5 | 2.5 | 2.5 | 100% |
| 02-Dec | NQ | 4,790.5 | 4,793.0 | 2.5 | 2.5 | 100% |
| 02-Dec | NQ | 4,793.0 | 4,797.0 | 4.0 | 4.0 | 100% |
| 02-Dec | NQ | 4,797.0 | 4,803.0 | 6.0 | 6.0 | 100% |
| 02-Dec | NQ | 4,803.0 | 4,812.0 | 9.0 | 9.0 | 100% |
| 04-Dec | NQ | 4,812.0 | 4,819.5 | 7.5 | 7.5 | 100% |
| 04-Dec | NQ | 4,819.5 | 4,829.5 | 10.0 | 10.0 | 100% |
| 04-Dec | NQ | 4,829.5 | 4,838.5 | 9.0 | 9.0 | 100% |
| 04-Dec | NQ | 4,838.5 | 4,848.5 | 10.0 | 10.0 | 100% |
| 04-Dec | NQ | 4,848.5 | 4,855.5 | 7.0 | 7.0 | 100% |
| 05-Dec | NQ | 4,855.5 | 4,865.5 | 10.0 | 10.0 | 100% |
| 05-Dec | NQ | 4,865.5 | 4,871.5 | 6.0 | 6.0 | 100% |
| 05-Dec | NQ | 4,871.5 | 4,872.5 | 1.0 | 1.0 | 100% |
| 05-Dec | NQ | 4,872.5 | 4,875.5 | 3.0 | 0.0 | 0% |
| 05-Dec | NQ | 4,875.5 | 4,879.0 | 3.5 | 0.0 | 0% |
| 05-Dec | NQ | 4,879.0 | 4,880.0 | 1.0 | 0.0 | 0% |
| 06-Dec | NQ | 4,880.0 | 4,880.5 | 0.5 | 0.5 | 100% |
| 06-Dec | NQ | 4,880.5 | 4,888.5 | 8.0 | 8.0 | 100% |
| 07-Dec | NQ | 4,888.5 | 4,904.0 | 15.5 | 10.0 | 65% |
| 07-Dec | NQ | 4,904.0 | 4,913.5 | 9.5 | 9.5 | 100% |
| 07-Dec | NQ | 4,913.5 | 4,920.5 | 7.0 | 7.0 | 100% |
| 07-Dec | NQ | 4,920.5 | 4,930.5 | 10.0 | 10.0 | 100% |
| 07-Dec | NQ | 4,930.5 | 4,941.0 | 10.5 | 10.0 | 95% |
| 08-Dec | NQ | 4,941.0 | 4,951.0 | 10.0 | 10.0 | 100% |
| 08-Dec | NQ | 4,951.0 | 4,961.0 | 10.0 | 10.0 | 100% |
| 08-Dec | NQ | 4,961.0 | 4,971.0 | 10.0 | 10.0 | 100% |
| 08-Dec | NQ | 4,971.0 | 4,981.0 | 10.0 | 10.0 | 100% |
| 08-Dec | NQ | 4,981.0 | 4,991.0 | 10.0 | 10.0 | 100% |
| 09-Dec | NQ | 4,991.0 | 5,001.0 | 10.0 | 10.0 | 100% |
| 09-Dec | NQ | 5,001.0 | 5,011.0 | 10.0 | 10.0 | 100% |
| 09-Dec | NQ | 5,011.0 | 5,021.0 | 10.0 | 10.0 | 100% |
| 09-Dec | NQ | 5,021.0 | 5,030.5 | 9.5 | 7.5 | 79% |
| 09-Dec | NQ | 5,030.5 | 5,034.5 | 4.0 | 4.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 09-Dec | NQ | 5,034.5 | 5,040.5 | 6.0 | 6.0 | 100% |
| 09-Dec | NQ | 5,040.5 | 5,043.5 | 3.0 | 2.0 | 67% |
| 10-Dec | NQ | 5,043.5 | 5,052.0 | 8.5 | 8.5 | 100% |
| 10-Dec | NQ | 5,052.0 | 5,055.5 | 3.5 | 3.5 | 100% |
| 10-Dec | NQ | 5,055.5 | 5,057.5 | 2.0 | 2.0 | 100% |
| 10-Dec | NQ | 5,057.5 | 5,061.0 | 3.5 | 3.5 | 100% |
| 10-Dec | NQ | 5,061.0 | 5,066.5 | 5.5 | 4.0 | 73% |
| 10-Dec | NQ | 5,066.5 | 5,067.5 | 1.0 | 1.0 | 100% |
| 10-Dec | NQ | 5,067.5 | 5,069.5 | 2.0 | 2.0 | 100% |
| 10-Dec | NQ | 5,069.5 | 5,072.5 | 3.0 | 2.5 | 83% |
| 10-Dec | NQ | 5,072.5 | 5,078.0 | 5.5 | 5.5 | 100% |
| 11-Dec | NQ | 5,078.0 | 5,083.0 | 5.0 | 5.0 | 100% |
| 11-Dec | NQ | 5,083.0 | 5,091.0 | 8.0 | 8.0 | 100% |
| 11-Dec | NQ | 5,091.0 | 5,095.0 | 4.0 | 4.0 | 100% |
| 11-Dec | NQ | 5,095.0 | 5,098.5 | 3.5 | 3.5 | 100% |
| 11-Dec | NQ | 5,098.5 | 5,108.5 | 10.0 | 9.0 | 90% |
| 11-Dec | NQ | 5,108.5 | 5,111.5 | 3.0 | 2.0 | 67% |
| 11-Dec | NQ | 5,111.5 | 5,114.5 | 3.0 | 0.5 | 17% |
| 11-Dec | NQ | 5,114.5 | 5,116.0 | 1.5 | 1.5 | 100% |
| 11-Dec | NQ | 5,116.0 | 5,116.5 | 0.5 | 0.5 | 100% |
| 12-Dec | NQ | 5,116.5 | 5,119.5 | 3.0 | 3.0 | 100% |
| 12-Dec | NQ | 5,119.5 | 5,123.0 | 3.5 | 3.5 | 100% |
| 12-Dec | NQ | 5,123.0 | 5,126.5 | 3.5 | 3.5 | 100% |
| 12-Dec | NQ | 5,126.5 | 5,135.0 | 8.5 | 8.5 | 100% |
| 12-Dec | NQ | 5,135.0 | 5,145.0 | 10.0 | 9.0 | 90% |
| 12-Dec | NQ | 5,145.0 | 5,155.0 | 10.0 | 10.0 | 100% |
| 12-Dec | NQ | 5,155.0 | 5,159.0 | 4.0 | 3.5 | 88% |
| 13-Dec | NQ | 5,159.0 | 5,163.0 | 4.0 | 4.0 | 100% |
| 13-Dec | NQ | 5,163.0 | 5,167.0 | 4.0 | 4.0 | 100% |
| 13-Dec | NQ | 5,167.0 | 5,173.0 | 6.0 | 3.0 | 50% |
| 13-Dec | NQ | 5,173.0 | 5,177.0 | 4.0 | 4.0 | 100% |
| 13-Dec | NQ | 5,177.0 | 5,180.5 | 3.5 | 3.0 | 86% |
| 13-Dec | NQ | 5,180.5 | 5,182.5 | 2.0 | 1.5 | 75% |
| 13-Dec | NQ | 5,182.5 | 5,190.5 | 8.0 | 8.0 | 100% |
| 13-Dec | NQ | 5,190.5 | 5,198.5 | 8.0 | 8.0 | 100% |
| 14-Dec | NQ | 5,198.5 | 5,203.5 | 5.0 | 5.0 | 100% |
| 14-Dec | NQ | 5,203.5 | 5,208.5 | 5.0 | 5.0 | 100% |
| 14-Dec | NQ | 5,208.5 | 5,218.5 | 10.0 | 10.0 | 100% |
| 14-Dec | NQ | 5,218.5 | 5,227.0 | 8.5 | 8.5 | 100% |
| 14-Dec | NQ | 5,227.0 | 5,237.0 | 10.0 | 10.0 | 100% |
| 14-Dec | NQ | 5,237.0 | 5,247.0 | 10.0 | 10.0 | 100% |
| 15-Dec | NQ | 5,247.0 | 5,267.0 | 20.0 | 10.0 | 50% |
| 15-Dec | NQ | 5,267.0 | 5,277.0 | 10.0 | 10.0 | 100% |
| 15-Dec | NQ | 5,277.0 | 5,287.0 | 10.0 | 10.0 | 100% |
| 15-Dec | NQ | 5,287.0 | 5,295.5 | 8.5 | 8.5 | 100% |
| 16-Dec | NQ | 5,295.5 | 5,305.5 | 10.0 | 10.0 | 100% |
| 16-Dec | NQ | 5,305.5 | 5,313.0 | 7.5 | 7.5 | 100% |
| 16-Dec | NQ | 5,313.0 | 5,322.0 | 9.0 | 9.0 | 100% |
| 16-Dec | NQ | 5,322.0 | 5,332.0 | 10.0 | 10.0 | 100% |

Table 2

SOH-1
Coring Performance

| Date | Core Size | Run Start | Run End | Footage Cored | Footage Recovered | Percent Recovery |
|---|---|---|---|---|---|---|
| 16-Dec | NQ | 5,332.0 | 5,342.0 | 10.0 | 10.0 | 100% |
| 17-Dec | NQ | 5,342.0 | 5,352.0 | 10.0 | 10.0 | 100% |
| 17-Dec | NQ | 5,352.0 | 5,362.0 | 10.0 | 10.0 | 100% |
| 17-Dec | NQ | 5,362.0 | 5,372.0 | 10.0 | 10.0 | 100% |
| 17-Dec | NQ | 5,372.0 | 5,382.0 | 10.0 | 10.0 | 100% |
| 18-Dec | NQ | 5,382.0 | 5,392.0 | 10.0 | 10.0 | 100% |
| 18-Dec | NQ | 5,392.0 | 5,402.0 | 10.0 | 10.0 | 100% |
| 18-Dec | NQ | 5,402.0 | 5,412.0 | 10.0 | 10.0 | 100% |
| 18-Dec | NQ | 5,412.0 | 5,422.0 | 10.0 | 10.0 | 100% |
| 19-Dec | NQ | 5,422.0 | 5,432.0 | 10.0 | 10.0 | 100% |
| 19-Dec | NQ | 5,432.0 | 5,442.0 | 10.0 | 10.0 | 100% |
| 19-Dec | NQ | 5,442.0 | 5,452.0 | 10.0 | 5.0 | 50% |
| 19-Dec | NQ | 5,452.0 | 5,456.5 | 4.5 | 4.0 | 89% |
| 20-Dec | NQ | 5,456.5 | 5,466.5 | 10.0 | 10.0 | 100% |
| 20-Dec | NQ | 5,466.5 | 5,476.5 | 10.0 | 10.0 | 100% |
| 20-Dec | NQ | 5,476.5 | 5,486.0 | 9.5 | 9.5 | 100% |
| 20-Dec | NQ | 5,486.0 | 5,496.0 | 10.0 | 10.0 | 100% |
| 20-Dec | NQ | 5,496.0 | 5,506.0 | 10.0 | 10.0 | 100% |
| 21-Dec | NQ | 5,506.0 | 5,516.0 | 10.0 | 10.0 | 100% |
| 21-Dec | NQ | 5,516.0 | 5,526.0 | 10.0 | 10.0 | 100% |
| | | Overall Totals | | 5,534.0 | 4,862.7 | 88% |

Table 3
SOH-1 Complaints

| # | Date | Resident | Complaint |
|---|---|---|---|
| 1 | JUN 1 | D. Pommerenk | Rig light shines in her window & sound gives her a headache. |
| 2 | JUN 4 | P. Majeska | Machine noise woke him up last night and was curious about source. |
| 3 | JUN 4 | D. Pommerenk | Noise complaint and is worried about permanent hearing damage. Also claims "hum in her head" caused by HGP-A has come back. |
| 4 | JUN 4 | B. Petricci | Noise complaint, "doesn't like it" and is "keeping notes." |
| 5 | JUN 4 | R. Jones | Noise wakes him up some nights, interested in measurements at Loughlins home. |
| 6 | JUN 13 | B. Gold | Light and noise complaint. |
| 7 | JUN 28 | D. Pommerenk | Noise complaint and wants combination to access road gate lock. |
| 8 | JUL 17 | D. Pommerenk | Noise complaint. |
| 9 | JUL 25 | B. Petricci | Noise complaint. |
| 10 | JUL 25 | D. Pommerenk | Noise complaint. |
| 11 | JUL 26 | D. Pommerenk | Noise complaint. |
| 12 | JUL 31 | D. Pommerenk | Noise complaint. |
| 13 | AUG 2 | G. Pommerenk | "Wants to know if its his imagination or is rig operation getting louder". |
| 14 | AUG 10 | D. Pommerenk | Noise complaint. |
| 15 | AUG 11 | D. Pommerenk | Claims 46db at her house, and "doesn't know how much more she can take". |
| 16 | AUG 28 | D. Pommerenk | Noise complaint. |
| 17 | AUG 28 | S. Phillips | Noise complaint. |
| 18 | SEP 3 | S. Phillips | Noise complaint. |

| # | Date | Resident | Complaint |
|---|---|---|---|
| 19 | SEP 3 | S. Phillips | Noise complaint |
| 20 | SEP 7 | D. Pommerenk | Noise complaint and complained because she couldn't reach crew on rig mobile phone. |
| 21 | SEP 24 | D. Pommerenk | Claims "SOH noise wakes children 3 times per week". |
| 22 | SEP 26 | D. Pommerenk | Noise complaint. |
| 23 | SEP 28 | S. Philips | Noise complaint. |
| 24 | OCT 9 | A. Sarhanis | Claims SOH noise wakes him up. |
| 25 | OCT 16 | D. Muller | Heard machinery noise one night, wanted to know what was going on. |
| 26 | OCT 21 | D. Pommerenk | SOH lights are shining in her window. |
| 27 | OCT 22 | D. Pommerenk | Noise complaint. |
| 28 | OCT 27 | D. Pommerenk | Noise complaint. |
| 29 | OCT 28 | D. Pommerenk | Noise complaint. |
| 30 | NOV 1 | D. Pommerenk | Noise complaint. |
| 31 | NOV 4 | D. Pommerenk | Noise complaint. |
| 32 | NOV 5 | D. Pommerenk | Noise complaint. |
| 33 | NOV 21 | D. Pommerenk | "Strange smell" around her house all day yesterday and "worse right now". |
| 34 | NOV 26 | D. Pommerenk | Noise complaint. |
| 35 | DEC 4 | G. Pommerenk | Noise complaint. |
| 36 | DEC 17 | D. Pommerenk | Noise complaint. |
| 37 | JAN 5 | D. Pommerenk | Noise complaint. |
| 38 | JAN 6 | D. Pommerenk | Noise complaint and claimed she read 50db on the noise meter she received for Christmas. |
| 39 | JAN 7 | D. Pommerenk | Noise complaint and claimed she read 52db on her noise meter. |
| 40 | JAN 7 | D. Pommerenk | Noise complaint. |

Table 4
SOH-1 Core Bits

| Bit # | Bit Size | S/N | Depth In | Depth Out | Footage Cut | Cost | Cost/ Foot | Cum. Bit Cost/ Foot | |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 101mm | 17700-3 | 0 | 381 | 381 | 1,016.00 | 2.67 | 2.67 | |
| 2 | 101mm | 17700-1 | 381 | 592 | 211 | 1,016.00 | 4.82 | 3.43 | |
| 3 | 101mm | 17700-5 | 592 | 730 | 138 | 1,016.00 | 7.36 | 4.18 | |
| 4 | 101mm | 17700-6 | 730 | 1,010 | 280 | 1,016.00 | 3.63 | 4.02 | |
| 5 | 101mm | 19925-6 | 1,010 | 1,034 | 24 | 858.00 | 35.75 | 4.76 | |
| 6 | 101mm | L-68514 | 1,034 | 1,115 | 81 | 858.00 | 10.59 | 5.18 | |
| 7 | 101mm | 17700-2 | 1,115 | 1,278 | 163 | 1,015.00 | 6.23 | 5.32 | |
| 8 | 101mm | 19999-3 | 1,278 | 1,459 | 181 | 949.00 | 5.24 | 5.31 | |
| 9 | 101mm | 19999-5 | 1,459 | 1,655 | 196 | 949.00 | 4.84 | 5.25 | |
| 10 | 101mm | 19999-4 | 1,655 | 1,996 | 341 | 949.00 | 2.78 | 4.83 | |
| 11 | 101mm | 19999-1 | 1,996 | 2,014 | 18 | 949.00 | 52.72 | 5.26 | |
| 12 | 101mm | 19999-2 | 2,014 | 2,074 | 60 | 1,016.00 | 16.93 | 5.60 | |
| 13 | 101mm | L-68517 | 2,074 | 2,201 | 127 | 1,016.00 | 8.00 | 5.74 | |
| 14 | 101mm | L-68515 | 2,201 | 2,331 | 130 | 1,016.00 | 7.82 | 5.85 | |
| 15 | 101mm | L-68516 | 2,331 | 2,481 | 150 | 1,016.00 | 6.77 | 5.91 | 101mm bit cost/ft. |
| 16 | 101mm | 19999-6 | 2,481 | 2,671 | 190 | 1,016.00 | 5.35 | 5.87 | $5.87 |
| 17 | 134mm | L-71870 | 2,671 | 2,717 | 46 | 1,759.00 | 38.24 | 6.42 | |
| 18 | 134mm | L-71871 | 2,717 | 2,768 | 51 | 1,759.00 | 34.49 | 6.93 | |
| 19 | 134mm | L-72641 | 2,768 | 2,851 | 83 | 1,643.00 | 19.80 | 7.31 | |
| 20 | 134mm | L-72642 | 2,851 | 2,868 | 17 | 1,643.00 | 96.65 | 7.84 | |
| 21 | 134mm | L-73246 | 2,868 | 2,884 | 16 | 1,759.00 | 109.94 | 8.40 | |
| 22 | 134mm | 73246 | 2,884 | 2,949 | 65 | 1,759.00 | 27.06 | 8.81 | 134mm bit cost/ft. |
| 23 | 134mm | 73370 | 2,949 | 3,022 | 73 | 1,759.00 | 24.10 | 9.18 | $34.42 |
| 24 | HQ | 3567419 | 3,022 | 3,231 | 209 | 785.66 | 3.76 | 8.83 | |
| 25 | HQ | M62357-1 | 3,231 | 3,305 | 74 | 555.26 | 7.50 | 8.80 | |
| 26 | HQ | L-63216 | 3,305 | 3,318 | 13 | 789.00 | 60.69 | 9.01 | |
| 27 | HQ | M63564-6 | 3,318 | 3,332 | 14 | 786.00 | 56.14 | 9.20 | |
| 28 | HQ | L-63213 | 3,332 | 3,368 | 36 | 789.00 | 21.92 | 9.34 | |
| 29 | HQ | M63564-10 | 3,368 | 3,399 | 31 | 786.00 | 25.35 | 9.49 | |
| 30 | HQ | L-3208 | 3,399 | 3,414 | 15 | 788.70 | 52.58 | 9.68 | |
| 31 | HQ | 15648-10 | 3,414 | 3,510 | 96 | 792.00 | 8.25 | 9.64 | |
| 32 | HQ | L-68480 | 3,510 | 3,512 | 2 | 801.90 | 400.95 | 9.86 | |
| 33 | HQ | M63564-24 | 3,512 | 3,529 | 17 | 785.66 | 46.22 | 10.03 | |
| 34 | HQ | L-68515 | 3,529 | 3,541 | 12 | 1,051.60 | 87.63 | 10.30 | |
| 35 | HQ | M63564-11 | 3,541 | 3,550 | 9 | 785.66 | 87.30 | 10.49 | |
| 36 | HQ | 71942-2 | 3,550 | 3,564 | 14 | 842.85 | 60.20 | 10.69 | |
| 37 | HQ | X9-956 | 3,564 | 3,625 | 61 | 918.50 | 15.06 | 10.76 | |
| 38 | HQ | 68474 | 3,625 | 3,726 | 101 | 843.70 | 8.35 | 10.70 | |
| 39 | HQ | 19993-8 | 3,726 | 3,870 | 144 | 800.20 | 5.56 | 10.50 | |
| 40 | HQ | 20180-3 | 3,870 | 3,922 | 52 | 816.64 | 15.70 | 10.57 | |
| 41 | HQ | 20180-6 | 3,922 | 3,980 | 58 | 816.64 | 14.08 | 10.62 | |
| 42 | HQ | M6-0309-3 | 3,980 | 4,025 | 45 | 785.66 | 17.46 | 10.70 | |
| 43 | HQ | M4-0308-2 | 4,025 | 4,064 | 39 | 785.66 | 20.15 | 10.79 | |
| 44 | HQ | M4-0308-3 | 4,064 | 4,098 | 34 | 785.66 | 23.11 | 10.89 | |

Table 4
SOH-1 Core Bits

| Bit # | Bit Size | S/N | Depth In | Depth Out | Footage Cut | Cost | Cost/ Foot | Cum. Bit Cost/ Foot | |
|---|---|---|---|---|---|---|---|---|---|
| 45 | HQ | M4-0308-1 | 4,098 | 4,120 | 22 | 785.66 | 35.71 | 11.03 | |
| 46 | HQ | 20180-2 | 4,120 | 4,135 | 15 | 816.64 | 54.44 | 11.18 | |
| 47 | HQ | M4-0308-4 | 4,135 | 4,167 | 32 | 785.66 | 24.55 | 11.29 | |
| 48 | HQ | BL-20180-1 | 4,167 | 4,182 | 15 | 816.64 | 54.44 | 11.44 | |
| 49 | HQ | OS-8387 | 4,182 | 4,214 | 32 | 673.20 | 21.04 | 11.51 | |
| 50 | HQ | OS-8396 | 4,214 | 4,236 | 22 | 673.24 | 30.60 | 11.61 | |
| 51 | HQ | L-77550 | 4,236 | 4,260 | 24 | 843.70 | 35.15 | 11.75 | |
| 52 | HQ | OS-8399 | 4,260 | 4,302 | 42 | 673.20 | 16.03 | 11.79 | |
| 53 | HQ | OS-8397 | 4,302 | 4,324 | 22 | 673.20 | 30.60 | 11.88 | HQ bit cost/ft. |
| 54 | HQ | L-77689 | 4,324 | 4,324 | 0 | 843.70 | N/A | 12.08 | $18.80 |
| 55 | NQ | L-33201 | 4,324 | 4,334 | 10 | 627.00 | 62.70 | 12.20 | |
| 56 | NQ | 9809-5 | 4,334 | 4,364 | 30 | 482.69 | 16.09 | 12.22 | |
| 57 | NQ | MX5-6583-4 | 4,364 | 4,364 | 0 | 481.60 | N/A | 12.33 | |
| 58 | NQ | L-74607 | 4,364 | 4,597 | 233 | 627.00 | 2.69 | 11.84 | |
| 59 | NQ | OS-10589 | 4,597 | 4,699 | 102 | 559.75 | 5.49 | 11.71 | |
| 60 | NQ | L-74606 | 4,699 | 4,812 | 113 | 627.00 | 5.55 | 11.56 | |
| 61 | NQ | L-67694 | 4,812 | 4,880 | 68 | 576.40 | 8.48 | 11.52 | NQ bit cost/ft |
| 62 | NQ | L-67701 | 4,880 | 5,526 | 646 | 576.40 | 0.89 | 10.28 | $3.79 |
| | | | | Total Bit Cost | | $56,786.63 | | | |

Bits used for reaming over stuck drill rods

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 1 | 134mm | L-71770 | 1,996 | 2,016 | 20 | 1,609.00 | 80.45 | |
| 2 | 134mm | L-71794 | 2,016 | 2,029 | 13 | 2,385.00 | 183.46 | |
| 3 | 134mm | L-71795 | 2,029 | 2,063 | 34 | 2,385.00 | 70.15 | |
| 4 | 134mm | L-71923 | 2,063 | 2,072 | 9 | 1,342.00 | 149.11 | |
| 5 | 134mm | L-71924 | 2,072 | 2,123 | 51 | 1,324.00 | 25.96 | |
| 6 | 134mm | L-71925 | 2,123 | 2,218 | 95 | 1,342.00 | 14.13 | |
| 7 | 134mm | L-71926 | 2,218 | 2,230 | 12 | 1,342.00 | 111.83 | |
| | | | | Total Reaming Bit Cost | | $11,729.00 | | |

Coring stabalizers, reamers
& other down hole consumable items. $30,988.94

Total bits & other down hole consumables. $99,504.57

Table 5
SOH DRILLING EXPENDITURES

| ACTIVITY | SOH-1 COST | SOH-1 % TOTAL | SOH-4 COST | SOH-4 % TOTAL |
|---|---|---|---|---|
| SITE & ROAD CONSTRUCTION | 5,589 | 0.34% | 4,500 | 0.31% |
| MOB, PREP. & SET-UP | 17,621 | 1.07% | 23,099 | 1.57% |
| RIG, LABOR, FOOTAGE CHG. & TAX | 961,614 | 58.51% | 735,347 | 50.13% |
| RENTAL EUIPMENT | 138,732 | 8.44% | 105,468 | 7.19% |
| BITS (core and rotary) | 73,569 | 4.48% | 35,775 | 2.44% |
| MISC. DOWN HOLE EQUIP. | 30,989 | 1.89% | 36,297 | 2.47% |
| MUDS | 91,810 | 5.59% | 94,534 | 6.44% |
| WATER (trucking & county charges) | 16,401 | 1.00% | 91,972 | 6.27% |
| CMT. & CMT SERVICES | 33,525 | 2.04% | 36,029 | 2.46% |
| WELLHEAD, CASING & FLOAT EQUIP. | 87,890 | 5.35% | 96,651 | 6.59% |
| BOP EQUIP. (Rental equipment) | 52,921 | 3.22% | 29,693 | 2.02% |
| TRANSPORTATION | 10,254 | 0.62% | 18,524 | 1.26% |
| MISC MATERIALS | 8,770 | 0.53% | 8,577 | 0.58% |
| MISC LABOR & SERVICES | 11,461 | 0.70% | 10,266 | 0.70% |
| SUPERVISION | 82,200 | 5.00% | 58,800 | 4.01% |
| GEOPHYSICAL LOGGING | 0 | 0.00% | 58,445 | 3.98% |
| OTHER | 20,198 | 1.23% | 22,836 | 1.56% |
| TOTAL EXPENDITURES | 1,643,544 | | 1,466,813 | |

Table 6
SOH-1
DRILLING COSTS AND ACTIVITIES

| Activity | Date | Day Number | Footage Start | Footage End | Daily Footage | Daily Cost | Cost-to Date | |
|---|---|---|---|---|---|---|---|---|
| Mob & set-up | May 1 - 31 | 0 | | 0 | | 42,916 | 42,916 | SITE CONSTRUCTION, |
| Core 101mm | 01-Jun | 1 | 0 | 122 | 122 | 10,057 | 52,973 | MOB & SET-UP |
| Core 101 & open 12.5" | 02-Jun | 2 | 122 | 202 | 80 | 8,079 | 61,052 | Total Cost $42,916 |
| Open 12-1/2" | 03-Jun | 3 | 30 | 100 | 0 | 7,090 | 68,142 | |
| Open 12-1/2" | 04-Jun | 4 | 100 | 188 | 0 | 7,725 | 75,867 | |
| Open 12-1/2" case & cmt | 05-Jun | 5 | 188 | 202 | 0 | 10,163 | 86,030 | |
| Cmt | 06-Jun | 6 | 202 | 202 | 0 | 5,539 | 91,569 | CORE, OPEN TO 12-1/4" |
| Cmt | 07-Jun | 7 | 202 | 202 | 0 | 7,591 | 99,160 | CASE & CEMENT (0 - 212 ft) |
| Cmt | 08-Jun | 8 | 202 | 202 | 0 | 5,316 | 104,476 | 202 ft. @ $66,972 |
| Cmt, test BOP | 09-Jun | 9 | 202 | 202 | 0 | 5,412 | 109,888 | Cost/foot $331.54 |
| Wait on county | 10-Jun | 10 | 202 | 202 | 0 | 5,142 | 115,030 | |
| Wait on county | 11-Jun | 11 | 202 | 202 | 0 | 5,057 | 120,087 | |
| Wait on county | 12-Jun | 12 | 202 | 202 | 0 | 5,066 | 125,153 | |
| Wait on county | 13-Jun | 13 | 202 | 202 | 0 | 5,057 | 130,210 | DELAY - COUNTY OF HAWAII |
| Wait on county | 14-Jun | 14 | 202 | 202 | 0 | 5,093 | 135,303 | Total Cost $29,061 |
| Wait & core 101mm | 15-Jun | 15 | 202 | 290 | 88 | 7,292 | 142,595 | |
| Core 101mm | 16-Jun | 16 | 290 | 433 | 143 | 8,473 | 151,068 | |
| Core 101mm | 17-Jun | 17 | 433 | 563 | 130 | 7,849 | 158,917 | |
| Core 101mm | 18-Jun | 18 | 563 | 669 | 106 | 7,986 | 166,903 | |
| Core 101mm | 19-Jun | 19 | 669 | 755 | 86 | 8,449 | 175,352 | |
| Core 101mm | 20-Jun | 20 | 755 | 874 | 119 | 7,101 | 182,453 | |
| Core 101mm | 21-Jun | 21 | 874 | 984 | 110 | 7,554 | 190,007 | |
| Core 101mm | 22-Jun | 22 | 984 | 1,040 | 56 | 8,673 | 198,680 | |
| Core 101mm | 23-Jun | 23 | 1,040 | 1,142 | 102 | 8,003 | 206,683 | |
| Core 101mm | 24-Jun | 24 | 1,142 | 1,245 | 103 | 7,322 | 214,005 | |
| Core 101mm | 25-Jun | 25 | 1,245 | 1,334 | 89 | 8,212 | 222,217 | |
| Core 101mm | 26-Jun | 26 | 1,334 | 1,418 | 84 | 6,890 | 229,107 | |
| Core 101mm | 27-Jun | 27 | 1,418 | 1,508 | 90 | 8,256 | 237,363 | |
| Core 101mm | 28-Jun | 28 | 1,508 | 1,615 | 107 | 7,865 | 245,228 | |
| Core 101mm | 29-Jun | 29 | 1,615 | 1,709 | 94 | 8,215 | 253,443 | CORE 101mm (202 - 1995 ft) |
| Core 101mm | 30-Jun | 30 | 1,709 | 1,802 | 93 | 7,685 | 261,128 | 1,793 ft. @ $136,457 |
| Core 101mm | 01-Jul | 31 | 1,802 | 1,911 | 109 | 7,327 | 268,455 | Cost/foot $76.11 |
| Core 101mm dev sur. | 02-Jul | 32 | 1,911 | 1,996 | 85 | 6,951 | 275,406 | |
| Open 8.5" | 03-Jul | 33 | 202 | 271 | 69 | 11,479 | 286,885 | |
| Open 8.5" | 04-Jul | 34 | 271 | 432 | 161 | 7,002 | 293,887 | |
| Open 8.5" | 05-Jul | 35 | 432 | 549 | 117 | 6,441 | 300,328 | |
| Open 8.5" & cmt back | 06-Jul | 36 | 549 | 555 | 6 | 8,344 | 308,672 | |
| Drl cmt 253 - 430 ft. | 07-Jul | 37 | 555 | 555 | 0 | 8,072 | 316,744 | |
| Drl cmt & open 8.5" | 08-Jul | 38 | 555 | 573 | 18 | 7,830 | 324,574 | |
| Open 8.5" | 09-Jul | 39 | 573 | 590 | 17 | 8,393 | 332,967 | |
| Down for repairs. | 10-Jul | 40 | 590 | 590 | 0 | 5,363 | 338,330 | |
| Repairs & open 8.5" | 11-Jul | 41 | 590 | 621 | 31 | 5,917 | 344,247 | |
| Open 8.5" cmt & drl cmt | 12-Jul | 42 | 621 | 629 | 8 | 7,645 | 351,892 | |
| Drl cmt 290 - 583 ft. | 13-Jul | 43 | 629 | 629 | 0 | 6,206 | 358,098 | |
| Drl cmt & open 8.5" | 14-Jul | 44 | 629 | 770 | 141 | 6,770 | 364,868 | |
| Open 8.5" & cmt back | 15-Jul | 45 | 770 | 796 | 26 | 7,670 | 372,538 | |

Table 6
SOH-1
DRILLING COSTS AND ACTIVITIES

| Activity | Date | Day Number | Footage Start | Footage End | Daily Footage | Daily Cost | Cost-to Date | |
|---|---|---|---|---|---|---|---|---|
| Drl cmt & open 8.5" | 16-Jul | 46 | 796 | 870 | 74 | 6,684 | 379,222 | |
| Open 8.5" | 17-Jul | 47 | 870 | 1,023 | 153 | 7,817 | 387,039 | |
| Open 8.5" | 18-Jul | 48 | 1,023 | 1,180 | 157 | 7,943 | 394,982 | |
| Open 8.5" cmt & drl cmt | 19-Jul | 49 | 1,180 | 1,200 | 20 | 7,815 | 402,797 | |
| Drl cmt & open 8.5" | 20-Jul | 50 | 1,200 | 1,298 | 98 | 6,950 | 409,747 | |
| Open 8.5" | 21-Jul | 51 | 1,298 | 1,412 | 114 | 6,690 | 416,437 | |
| Open 8.5" | 22-Jul | 52 | 1,412 | 1,574 | 162 | 7,548 | 423,985 | |
| Open 8.5" | 23-Jul | 53 | 1,574 | 1,731 | 157 | 6,808 | 430,793 | |
| Open 8.5" | 24-Jul | 54 | 1,731 | 1,820 | 89 | 6,401 | 437,194 | |
| Open 8.5" | 25-Jul | 55 | 1,820 | 1,958 | 138 | 7,171 | 444,365 | |
| Open 8.5" lay dn rods | 26-Jul | 56 | 1,958 | 1,996 | 38 | 6,634 | 450,999 | |
| Run csg, drop, fish. | 27-Jul | 57 | 1,996 | 1,996 | 0 | 6,260 | 457,259 | |
| Fishing | 28-Jul | 58 | 1,996 | 1,996 | 0 | 6,045 | 463,304 | OPEN HOLE, FISH, CASE & |
| Fish, rig for cmt | 29-Jul | 59 | 1,996 | 1,996 | 0 | 40,677 | 503,981 | CEMENT (202 - 1,996 ft) |
| Cmt | 30-Jul | 60 | 1,996 | 1,996 | 0 | 33,333 | 537,314 | 1,794 ft. @ $268,742 |
| Rig BOP, test, drl cmt | 31-Jul | 61 | 1,996 | 1,996 | 0 | 6,834 | 544,148 | Cost/foot $149.80 |
| Drl cmt, core 101mm | 01-Aug | 62 | 1,996 | 2,014 | 18 | 7,345 | 551,493 | |
| Core 101mm | 02-Aug | 63 | 2,014 | 2,074 | 60 | 5,889 | 557,382 | |
| Core 101mm | 03-Aug | 64 | 2,074 | 2,137 | 63 | 6,166 | 563,548 | |
| Core 101mm | 04-Aug | 65 | 2,137 | 2,201 | 64 | 6,215 | 569,763 | |
| Core 101mm | 05-Aug | 66 | 2,201 | 2,266 | 65 | 5,985 | 575,748 | |
| Core 101mm | 06-Aug | 67 | 2,266 | 2,368 | 102 | 7,644 | 583,392 | |
| Core 101mm | 07-Aug | 68 | 2,368 | 2,481 | 113 | 7,891 | 591,283 | |
| Core 101mm & cmt back | 08-Aug | 69 | 2,481 | 2,505 | 24 | 5,891 | 597,174 | |
| Drl out cmt. | 09-Aug | 70 | 2,505 | 2,505 | 0 | 6,394 | 603,568 | |
| Drl out cmt. | 10-Aug | 71 | 2,505 | 2,505 | 0 | 4,853 | 608,421 | CORE 101mm (1,996 - 2,671 ft) |
| Core 101mm | 11-Aug | 72 | 2,505 | 2,645 | 140 | 8,438 | 616,859 | 675 ft. @ $84,463 |
| Core 101mm & cmt back | 12-Aug | 73 | 2,645 | 2,671 | 26 | 5,878 | 622,737 | Cost/foot $125.13 |
| RIH, stick rods | 13-Aug | 74 | 2,671 | 2,671 | 0 | 5,874 | 628,611 | |
| RIH, cut rods | 14-Aug | 75 | 2,671 | 2,671 | 0 | 5,494 | 634,105 | |
| Cut & jar rods | 15-Aug | 76 | 2,671 | 2,671 | 0 | 6,833 | 640,938 | |
| make up 134mm rods | 16-Aug | 77 | 2,671 | 2,671 | 0 | 6,540 | 647,478 | |
| Ream over w/ 134mm | 17-Aug | 78 | 1,996 | 2,009 | 13 | 8,010 | 655,488 | |
| Ream over w/ 134mm | 18-Aug | 79 | 2,009 | 2,024 | 15 | 9,222 | 664,710 | |
| Ream over w/ 134mm | 19-Aug | 80 | 2,024 | 2,039 | 15 | 9,485 | 674,195 | |
| Ream over w/ 134mm | 20-Aug | 81 | 2,039 | 2,060 | 21 | 6,980 | 681,175 | |
| Ream over w/ 134mm | 21-Aug | 82 | 2,060 | 2,063 | 3 | 5,799 | 686,974 | |
| Ream over w/ 134mm | 22-Aug | 83 | 2,063 | 2,072 | 9 | 9,338 | 696,312 | |
| Ream over w/ 134mm | 23-Aug | 84 | 2,072 | 2,086 | 14 | 7,704 | 704,016 | |
| Ream over w/ 134mm | 24-Aug | 85 | 2,086 | 2,118 | 32 | 6,670 | 710,686 | |
| Ream over w/ 134mm | 25-Aug | 86 | 2,118 | 2,138 | 20 | 7,607 | 718,293 | |
| Ream over w/ 134mm | 26-Aug | 87 | 2,138 | 2,170 | 32 | 6,669 | 724,962 | |
| Ream over w/ 134mm | 27-Aug | 88 | 2,170 | 2,213 | 43 | 6,424 | 731,386 | |
| Ream over w/ 134mm | 28-Aug | 89 | 2,213 | 2,218 | 5 | 7,784 | 739,170 | |
| Ream over w/ 134mm | 29-Aug | 90 | 2,218 | 2,230 | 12 | 6,402 | 745,572 | |
| Fish out 101mm rods | 30-Aug | 91 | 2,230 | 2,230 | 0 | 5,925 | 751,497 | |

Table 6
SOH-1
DRILLING COSTS AND ACTIVITIES

| Activity | Date | Day Number | Footage Start | Footage End | Daily Footage | Daily Cost | Cost-to Date | |
|---|---|---|---|---|---|---|---|---|
| Fish & open 5-7/8" hole | 31-Aug | 92 | 1,996 | 2,010 | 14 | 13,053 | 764,550 | |
| Open 5-7/8" hole | 01-Sep | 93 | 2,010 | 2,082 | 72 | 5,835 | 770,385 | |
| Open 5-7/8" hole | 02-Sep | 94 | 2,082 | 2,152 | 70 | 6,041 | 776,426 | |
| Open 5-7/8" hole | 03-Sep | 95 | 2,152 | 2,183 | 31 | 6,897 | 783,323 | |
| Open 5-7/8" hole | 04-Sep | 96 | 2,183 | 2,277 | 94 | 6,223 | 789,546 | |
| Open 5-7/8" hole | 05-Sep | 97 | 2,277 | 2,369 | 92 | 6,484 | 796,030 | |
| Open 5-7/8" hole | 06-Sep | 98 | 2,369 | 2,451 | 82 | 6,655 | 802,685 | FISH, REAM OVER STUCK RODS |
| Open 5-7/8" hole & wash | 07-Sep | 99 | 2,451 | 2,506 | 55 | 7,834 | 810,519 | & OPEN HOLE TO 5-5/8" |
| Wash hole | 08-Sep | 100 | 2,506 | 2,506 | 0 | 6,328 | 816,847 | (1,996 - 2,671 ft) |
| Open 5-7/8" hole | 09-Sep | 101 | 2,506 | 2,600 | 94 | 6,916 | 823,763 | Total Cost $201,709 |
| Open hole, stick rods | 10-Sep | 102 | 2,600 | 2,671 | 71 | 6,557 | 830,320 | |
| POH, core 134mm | 11-Sep | 103 | 2,671 | 2,717 | 46 | 10,316 | 840,636 | |
| Core 134mm | 12-Sep | 104 | 2,717 | 2,738 | 21 | 8,191 | 848,827 | |
| Core 134mm | 13-Sep | 105 | 2,738 | 2,770 | 32 | 8,172 | 856,999 | |
| Core 134mm | 14-Sep | 106 | 2,770 | 2,836 | 66 | 6,691 | 863,690 | |
| Core 134mm | 15-Sep | 107 | 2,836 | 2,865 | 29 | 8,394 | 872,084 | |
| Core 134mm | 16-Sep | 108 | 2,865 | 2,868 | 3 | 7,919 | 880,003 | |
| Core 134mm | 17-Sep | 109 | 2,868 | 2,896 | 28 | 9,167 | 889,170 | CORE 134mm 2,671 - 3,022 ft |
| Core 134mm | 18-Sep | 110 | 2,896 | 2,935 | 39 | 6,960 | 896,130 | & SET 4-1/2" CSG. |
| Core 134mm | 19-Sep | 111 | 2,935 | 2,957 | 22 | 8,648 | 904,778 | 351 ft. @ $73,047 |
| Core 134mm | 20-Sep | 112 | 2,957 | 2,993 | 36 | 6,802 | 911,580 | Cost/foot $208.11 |
| Core 134mm | 21-Sep | 113 | 2,993 | 3,022 | 29 | 7,717 | 919,297 | |
| Run & cmt 4.5" csg | 22-Sep | 114 | 3,022 | 3,022 | 0 | 7,096 | 926,393 | |
| WOC, core HQ | 23-Sep | 115 | 3,022 | 3,037 | 15 | 23,329 | 949,722 | CASING OPERATIONS |
| Core HQ | 24-Sep | 116 | 3,037 | 3,104 | 67 | 6,551 | 956,273 | 4-1/2" CASING 0 - 3,022 ft |
| Core HQ | 25-Sep | 117 | 3,104 | 3,172 | 68 | 6,221 | 962,494 | & CEMENT |
| Core HQ | 26-Sep | 118 | 3,172 | 3,231 | 59 | 6,784 | 969,278 | Total cost $23,026 |
| Core HQ | 27-Sep | 119 | 3,231 | 3,266 | 35 | 7,478 | 976,756 | |
| Core HQ | 28-Sep | 120 | 3,266 | 3,308 | 42 | 6,732 | 983,488 | |
| Core HQ | 29-Sep | 121 | 3,308 | 3,329 | 21 | 7,172 | 990,660 | |
| Core HQ | 30-Sep | 122 | 3,329 | 3,346 | 17 | 7,295 | 997,955 | |
| Core HQ | 01-Oct | 123 | 3,346 | 3,377 | 31 | 6,999 | 1,004,954 | |
| Core HQ | 02-Oct | 124 | 3,377 | 3,402 | 25 | 7,682 | 1,012,636 | |
| Core HQ | 03-Oct | 125 | 3,402 | 3,422 | 20 | 6,067 | 1,018,703 | |
| Core HQ | 04-Oct | 126 | 3,422 | 3,462 | 40 | 6,193 | 1,024,896 | |
| Core HQ | 05-Oct | 127 | 3,462 | 3,498 | 36 | 6,054 | 1,030,950 | |
| Core HQ | 06-Oct | 128 | 3,498 | 3,512 | 14 | 9,532 | 1,040,482 | |
| Core HQ | 07-Oct | 129 | 3,512 | 3,538 | 26 | 7,639 | 1,048,121 | |
| Core HQ | 08-Oct | 130 | 3,538 | 3,550 | 12 | 6,896 | 1,055,017 | |
| Core HQ | 09-Oct | 131 | 3,550 | 3,565 | 15 | 6,532 | 1,061,549 | |
| Core HQ | 10-Oct | 132 | 3,565 | 3,590 | 25 | 6,790 | 1,068,339 | |
| Core HQ | 11-Oct | 133 | 3,590 | 3,625 | 35 | 6,138 | 1,074,477 | |
| Core HQ | 12-Oct | 134 | 3,625 | 3,660 | 35 | 6,902 | 1,081,379 | |
| Core HQ | 13-Oct | 135 | 3,660 | 3,716 | 56 | 6,176 | 1,087,555 | |
| Core HQ | 14-Oct | 136 | 3,716 | 3,775 | 59 | 7,405 | 1,094,960 | |
| Core HQ | 15-Oct | 137 | 3,775 | 3,844 | 69 | 6,265 | 1,101,225 | |

Table 6
SOH-1
DRILLING COSTS AND ACTIVITIES

| Activity | Date | Day Number | Footage Start | Footage End | Daily Footage | Daily Cost | Cost-to Date | | |
|---|---|---|---|---|---|---|---|---|---|
| Core HQ | 16-Oct | 138 | 3,844 | 3,870 | 26 | 6,095 | 1,107,320 | | |
| Core HQ | 17-Oct | 139 | 3,870 | 3,892 | 22 | 7,423 | 1,114,743 | | |
| Core HQ | 18-Oct | 140 | 3,892 | 3,920 | 28 | 6,308 | 1,121,051 | | |
| Core HQ | 19-Oct | 141 | 3,920 | 3,934 | 14 | 7,024 | 1,128,075 | | |
| Core HQ | 20-Oct | 142 | 3,934 | 3,976 | 42 | 6,348 | 1,134,423 | | |
| Core HQ | 21-Oct | 143 | 3,976 | 3,992 | 16 | 7,033 | 1,141,456 | | |
| Core HQ | 22-Oct | 144 | 3,992 | 4,025 | 33 | 6,186 | 1,147,642 | | |
| Core HQ | 23-Oct | 145 | 4,025 | 4,037 | 12 | 7,661 | 1,155,303 | | |
| Core HQ | 24-Oct | 146 | 4,037 | 4,064 | 27 | 7,145 | 1,162,448 | | |
| Core HQ | 25-Oct | 147 | 4,064 | 4,081 | 17 | 7,908 | 1,170,356 | | |
| Core HQ | 26-Oct | 148 | 4,081 | 4,098 | 17 | 7,389 | 1,177,745 | | |
| Core HQ | 27-Oct | 149 | 4,098 | 4,113 | 15 | 6,492 | 1,184,237 | | |
| Core HQ | 28-Oct | 150 | 4,113 | 4,120 | 7 | 7,156 | 1,191,393 | | |
| Core HQ | 29-Oct | 151 | 4,120 | 4,135 | 15 | 7,423 | 1,198,816 | | |
| Core HQ | 30-Oct | 152 | 4,135 | 4,167 | 32 | 6,546 | 1,205,362 | | |
| Core HQ | 31-Oct | 153 | 4,167 | 4,181 | 14 | 7,602 | 1,212,964 | | |
| Core HQ | 01-Nov | 154 | 4,181 | 4,188 | 7 | 7,187 | 1,220,151 | | |
| Core HQ | 02-Nov | 155 | 4,188 | 4,214 | 26 | 6,121 | 1,226,272 | | |
| Core HQ | 03-Nov | 156 | 4,214 | 4,226 | 12 | 6,771 | 1,233,043 | | |
| Core HQ | 04-Nov | 157 | 4,226 | 4,236 | 10 | 8,342 | 1,241,385 | | |
| Core HQ | 05-Nov | 158 | 4,236 | 4,248 | 12 | 5,940 | 1,247,325 | | |
| Core HQ | 06-Nov | 159 | 4,248 | 4,260 | 12 | 6,538 | 1,253,863 | | |
| Core HQ | 07-Nov | 160 | 4,260 | 4,287 | 27 | 6,037 | 1,259,900 | | |
| Core HQ | 08-Nov | 161 | 4,287 | 4,302 | 15 | 6,817 | 1,266,717 | CORE HQ (3,022 - 4,325 FT) | |
| Core HQ | 09-Nov | 162 | 4,302 | 4,307 | 5 | 6,025 | 1,272,742 | 1,303 ft. @ | $360,154 |
| Core HQ | 10-Nov | 163 | 4,307 | 4,324 | 17 | 6,884 | 1,279,626 | Cost/foot | $276.40 |
| Reduce to NQ | 11-Nov | 164 | 4,324 | 4,324 | 0 | 6,921 | 1,286,547 | | |
| Core NQ | 12-Nov | 165 | 4,324 | 4,334 | 10 | 6,124 | 1,292,671 | | |
| Core NQ | 13-Nov | 166 | 4,334 | 4,360 | 26 | 6,436 | 1,299,107 | | |
| Core NQ | 14-Nov | 167 | 4,360 | 4,364 | 4 | 6,748 | 1,305,855 | | |
| Core NQ | 15-Nov | 168 | 4,364 | 4,364 | 0 | 6,872 | 1,312,727 | | |
| Core NQ | 16-Nov | 169 | 4,364 | 4,387 | 23 | 7,078 | 1,319,805 | | |
| Core NQ | 17-Nov | 170 | 4,387 | 4,429 | 42 | 6,851 | 1,326,656 | | |
| Core NQ | 18-Nov | 171 | 4,429 | 4,460 | 31 | 7,162 | 1,333,818 | | |
| Core NQ | 19-Nov | 172 | 4,460 | 4,490 | 30 | 6,178 | 1,339,996 | | |
| Core NQ | 20-Nov | 173 | 4,490 | 4,530 | 40 | 6,415 | 1,346,411 | | |
| Core NQ | 21-Nov | 174 | 4,530 | 4,565 | 35 | 6,200 | 1,352,611 | | |
| Core NQ | 22-Nov | 175 | 4,565 | 4,595 | 30 | 6,398 | 1,359,009 | | |
| Core NQ | 23-Nov | 176 | 4,595 | 4,597 | 2 | 6,488 | 1,365,497 | | |
| Core NQ | 24-Nov | 177 | 4,597 | 4,602 | 5 | 7,950 | 1,373,447 | | |
| Core NQ | 25-Nov | 178 | 4,602 | 4,621 | 19 | 6,142 | 1,379,589 | | |
| Core NQ | 26-Nov | 179 | 4,621 | 4,650 | 29 | 6,348 | 1,385,937 | | |
| Core NQ | 27-Nov | 180 | 4,650 | 4,684 | 34 | 6,283 | 1,392,220 | | |
| Core NQ | 28-Nov | 181 | 4,684 | 4,699 | 15 | 6,834 | 1,399,054 | | |
| Core NQ | 29-Nov | 182 | 4,699 | 4,699 | 0 | 7,126 | 1,406,180 | | |
| Core NQ | 30-Nov | 183 | 4,699 | 4,723 | 24 | 6,753 | 1,412,933 | | |

Table 6
SOH-1
DRILLING COSTS AND ACTIVITIES

| Activity | Date | Day Number | Footage Start | Footage End | Daily Footage | Daily Cost | Cost-to Date | |
|---|---|---|---|---|---|---|---|---|
| Core NQ | 01-Dec | 184 | 4,723 | 4,753 | 30 | 6,462 | 1,419,395 | |
| Core NQ | 02-Dec | 185 | 4,753 | 4,777 | 24 | 6,365 | 1,425,760 | |
| Core NQ | 03-Dec | 186 | 4,777 | 4,812 | 35 | 6,262 | 1,432,022 | |
| Core NQ | 04-Dec | 187 | 4,812 | 4,812 | 0 | 6,483 | 1,438,505 | |
| Core NQ | 05-Dec | 188 | 4,812 | 4,855 | 43 | 6,815 | 1,445,320 | |
| Core NQ | 06-Dec | 189 | 4,855 | 4,880 | 25 | 6,667 | 1,451,987 | |
| Core NQ | 07-Dec | 190 | 4,880 | 4,888 | 8 | 6,557 | 1,458,544 | |
| Core NQ | 08-Dec | 191 | 4,888 | 4,941 | 53 | 6,164 | 1,464,708 | |
| Core NQ | 09-Dec | 192 | 4,941 | 4,991 | 50 | 6,128 | 1,470,836 | |
| Core NQ | 10-Dec | 193 | 4,991 | 5,043 | 52 | 6,191 | 1,477,027 | |
| Core NQ | 11-Dec | 194 | 5,043 | 5,078 | 35 | 5,852 | 1,482,879 | |
| Core NQ | 12-Dec | 195 | 5,078 | 5,116 | 38 | 5,901 | 1,488,780 | |
| Core NQ | 13-Dec | 196 | 5,116 | 5,159 | 43 | 6,044 | 1,494,824 | |
| Core NQ | 14-Dec | 197 | 5,159 | 5,198 | 39 | 6,349 | 1,501,173 | |
| Core NQ | 15-Dec | 198 | 5,198 | 5,247 | 49 | 6,032 | 1,507,205 | |
| Core NQ | 16-Dec | 199 | 5,247 | 5,295 | 48 | 5,842 | 1,513,047 | |
| Core NQ | 17-Dec | 200 | 5,295 | 5,342 | 47 | 5,951 | 1,518,998 | |
| Core NQ | 18-Dec | 201 | 5,342 | 5,382 | 40 | 5,875 | 1,524,873 | |
| Core NQ | 19-Dec | 202 | 5,382 | 5,422 | 40 | 5,799 | 1,530,672 | CORE NQ (4,325 - 5,526 FT) |
| Core NQ | 20-Dec | 203 | 5,422 | 5,456 | 34 | 5,641 | 1,536,313 | 1,201 ft. @ $258,989 |
| Core NQ | 21-Dec | 204 | 5,456 | 5,506 | 50 | 5,730 | 1,542,043 | Cost/foot $215.64 |
| TD hole, survey | 22-Dec | 205 | 5,506 | 5,526 | 20 | 3,493 | 1,545,536 | |
| Condition hole, shut in | 23-Dec | 206 | 5,526 | 5,526 | 0 | 2,986 | 1,548,522 | |
| Condition hole | 04-Jan | 207 | 5,526 | 5,526 | 0 | 10,518 | 1,559,040 | |
| Condition, standby | 05-Jan | 208 | 5,526 | 5,526 | 0 | 5,454 | 1,564,494 | |
| Run temp & press. logs | 06-Jan | 209 | 5,526 | 5,526 | 0 | 6,236 | 1,570,730 | |
| Run gam. & cal. logs | 07-Jan | 210 | 5,526 | 5,526 | 0 | 5,662 | 1,576,392 | |
| Lay dn rods, run tubing | 08-Jan | 211 | 5,526 | 5,526 | 0 | 30,657 | 1,607,049 | |
| Hang tubing, install w/h | 09-Jan | 212 | 5,526 | 5,526 | 0 | 13,357 | 1,620,406 | |
| Test, log & rig down | 10-Jan | 213 | 5,526 | 5,526 | 0 | 5,427 | 1,625,833 | |
| Loggine & rig down | 11-Jan | 214 | 5,526 | 5,526 | 0 | 5,115 | 1,630,948 | |
| Rig down & repairs | 12-Jan | 215 | 5,526 | 5,526 | 0 | 5,271 | 1,636,219 | COMPLETION, TESTING & |
| Rigging down | 13-Jan | 216 | 5,526 | 5,526 | 0 | 4,271 | 1,640,490 | RIG DOWN |
| Rig down & move | 14-Jan | 217 | 5,526 | 5,526 | 0 | 3,054 | 1,643,544 | Total Cost $98,008 |

TOTAL DRILLING COSTS: $1,643,544

Table 7

SOH-1
Hole Deviation Measurements

| Depth (feet) | Angle (degrees) | Bearing |
|---|---|---|
| 1,130 | 0.50 | S |
| 1,250 | 0.50 | S |
| 1,370 | 0.75 | S |
| 1,490 | 1.00 | S-5-E |
| 1,610 | 1.00 | S-5-E |
| 1,730 | 1.00 | S-10-E |
| 1,850 | 1.00 | S-10-E |
| 1,990 | 0.75 | S-10-W |
| 3,400 | 2.50 | S-40-W |

Figure 1

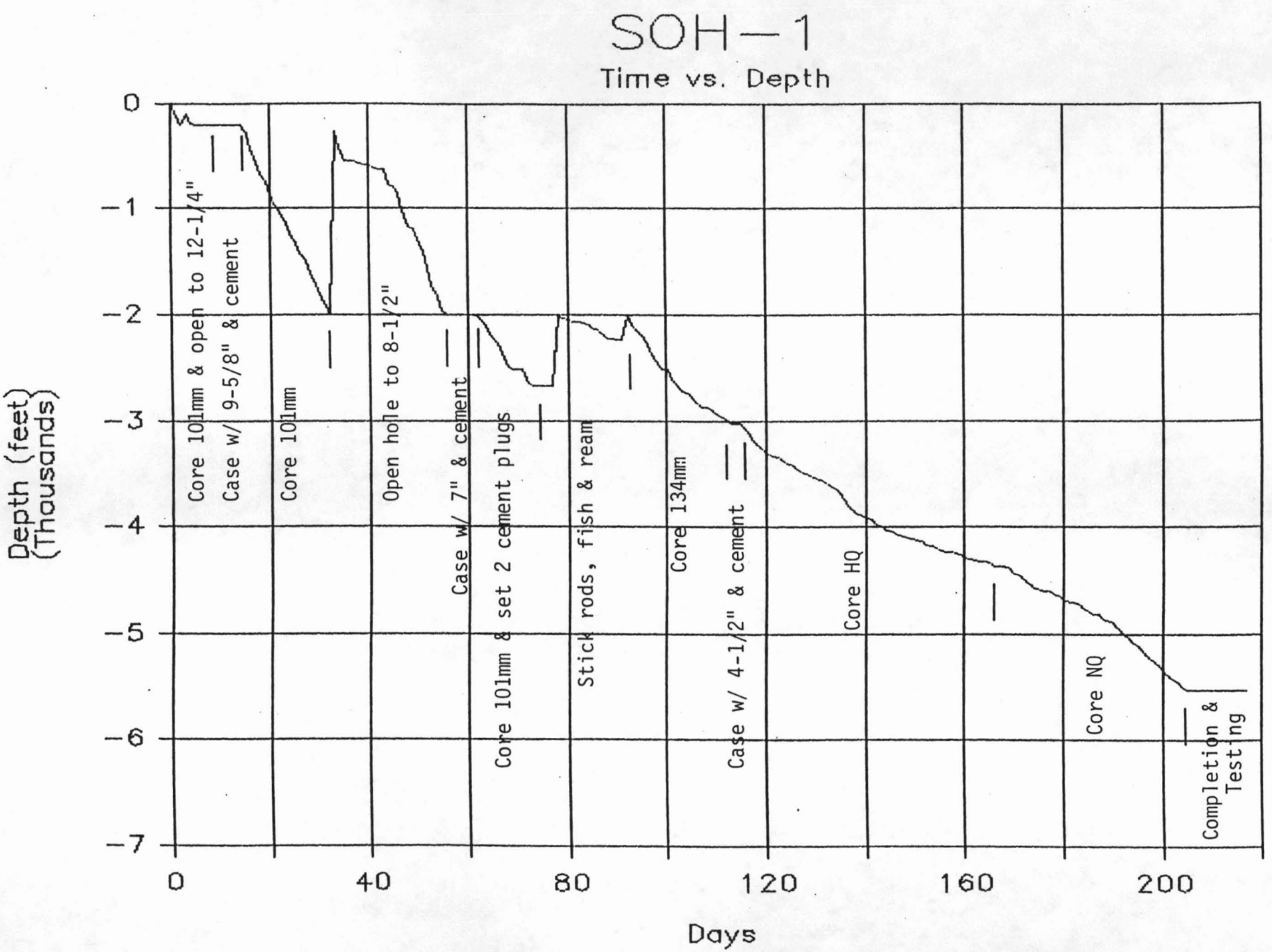

SOH-1
Time vs. Depth
Depth (feet)
(Thousands)
0
-1
-2
-3
-4
-5
-6
-7
0
40
80
120
160
200
Days
Core 101mm & open to 12-1/4"
Case w/ 9-5/8" & cement
Core 101mm
Open hole to 8-1/2"
Case w/ 7" & cement
Core 101mm & set 2 cement plugs
Stick rods, fish & ream
Core 134mm
Case w/ 4-1/2" & cement
Core HQ
Core NQ
Completion & Testing

Figure 2


SOH-1
Cost vs. Depth
0
-1
-2
-3
-4
-5
-6
-7
Depth - feet
(Thousands)
0
0.2
0.4
0.6
0.8
1
1.2
1.4
1.6
(Millions)
Cost

Figure 3

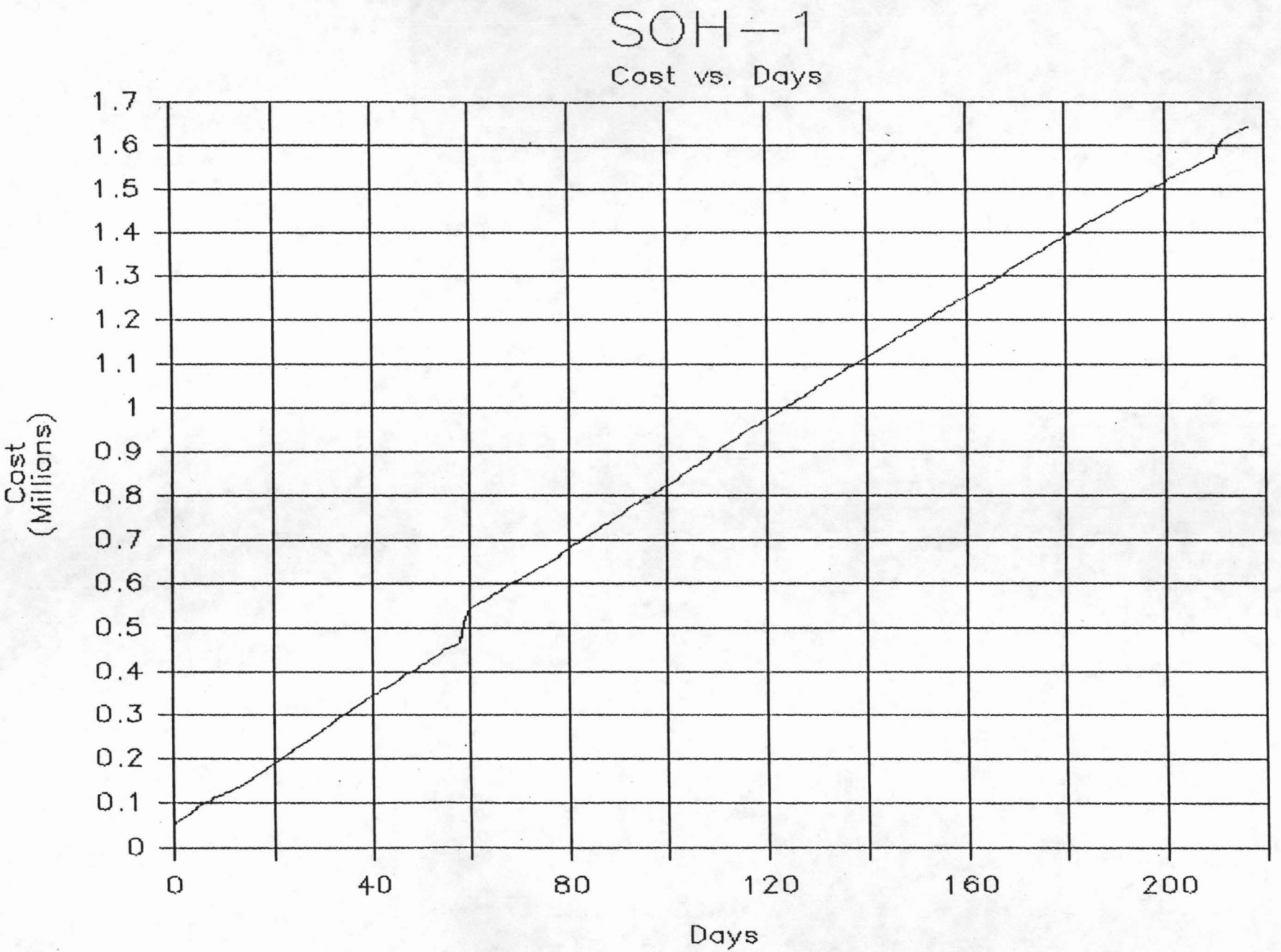

SOH-1
Cost vs. Days
Cost (Millions)
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
0
40
80
120
160
200
Days

Figure 4

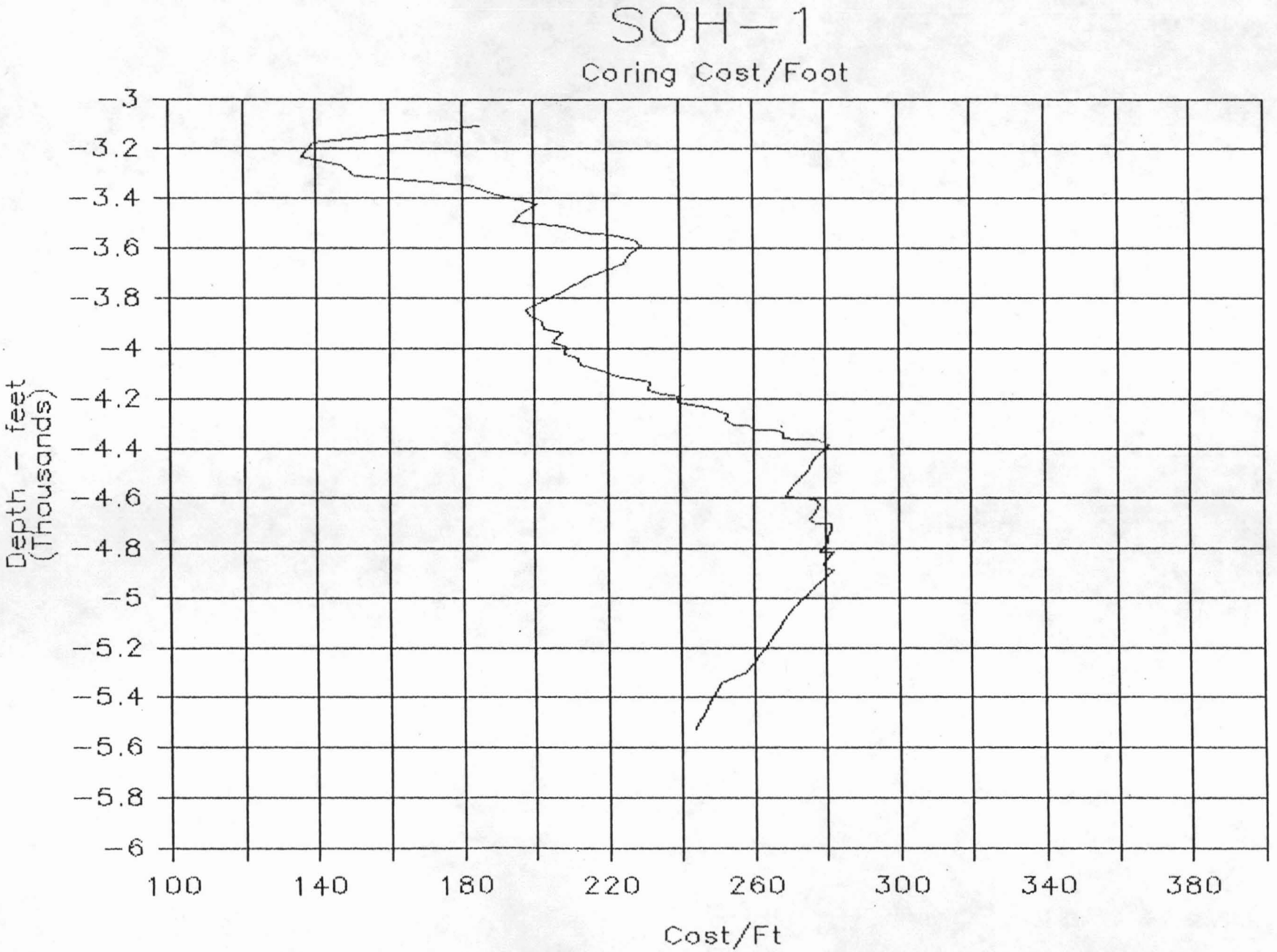

SOH-1
Coring Cost/Foot
-3
-3.2
-3.4
-3.6
-3.8
-4
-4.2
-4.4
-4.6
-4.8
-5
-5.2
-5.4
-5.6
-5.8
-6
Depth - feet (Thousands)
100
140
180
220
260
300
340
380
Cost/Ft

Figure 5

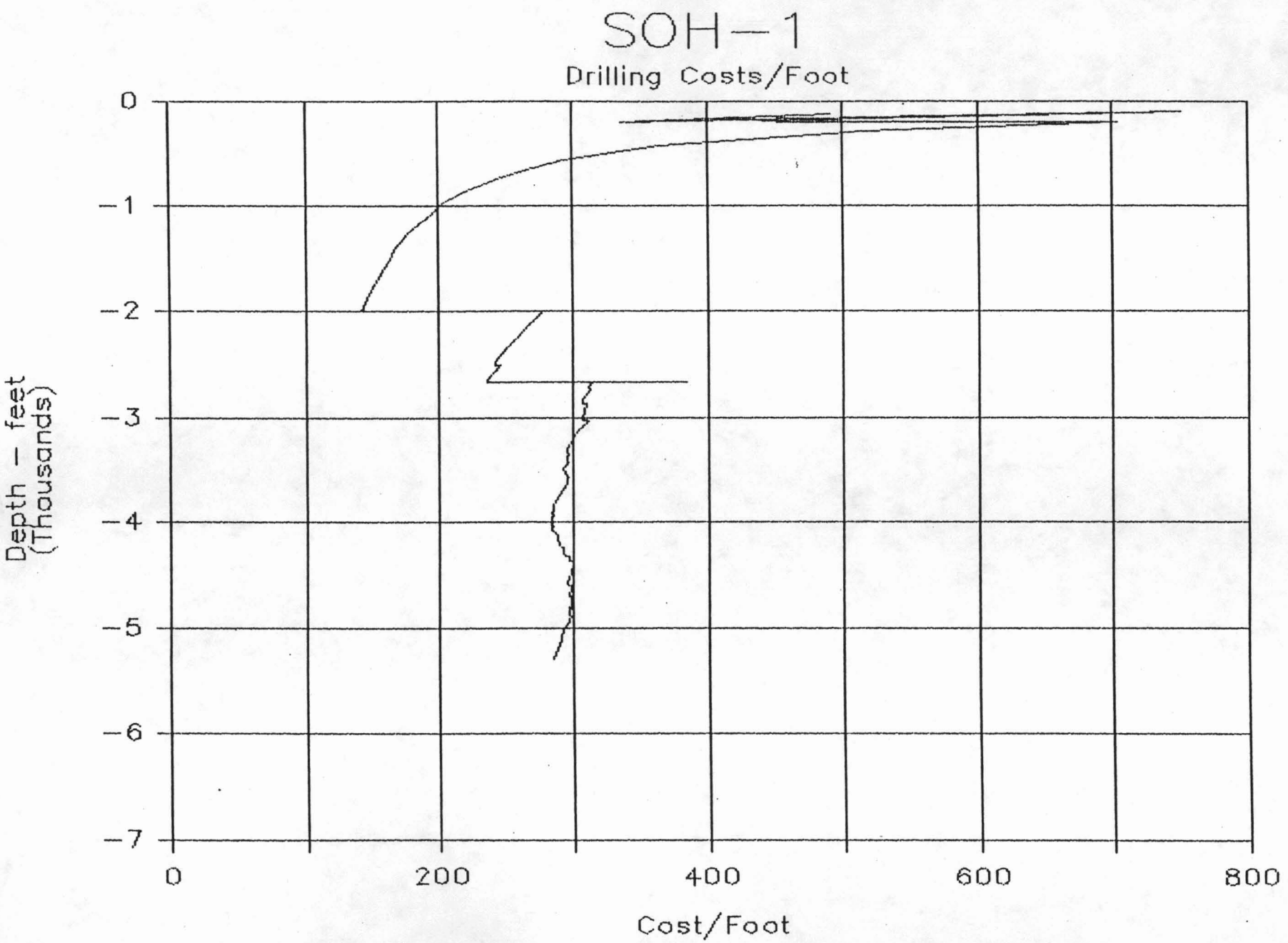
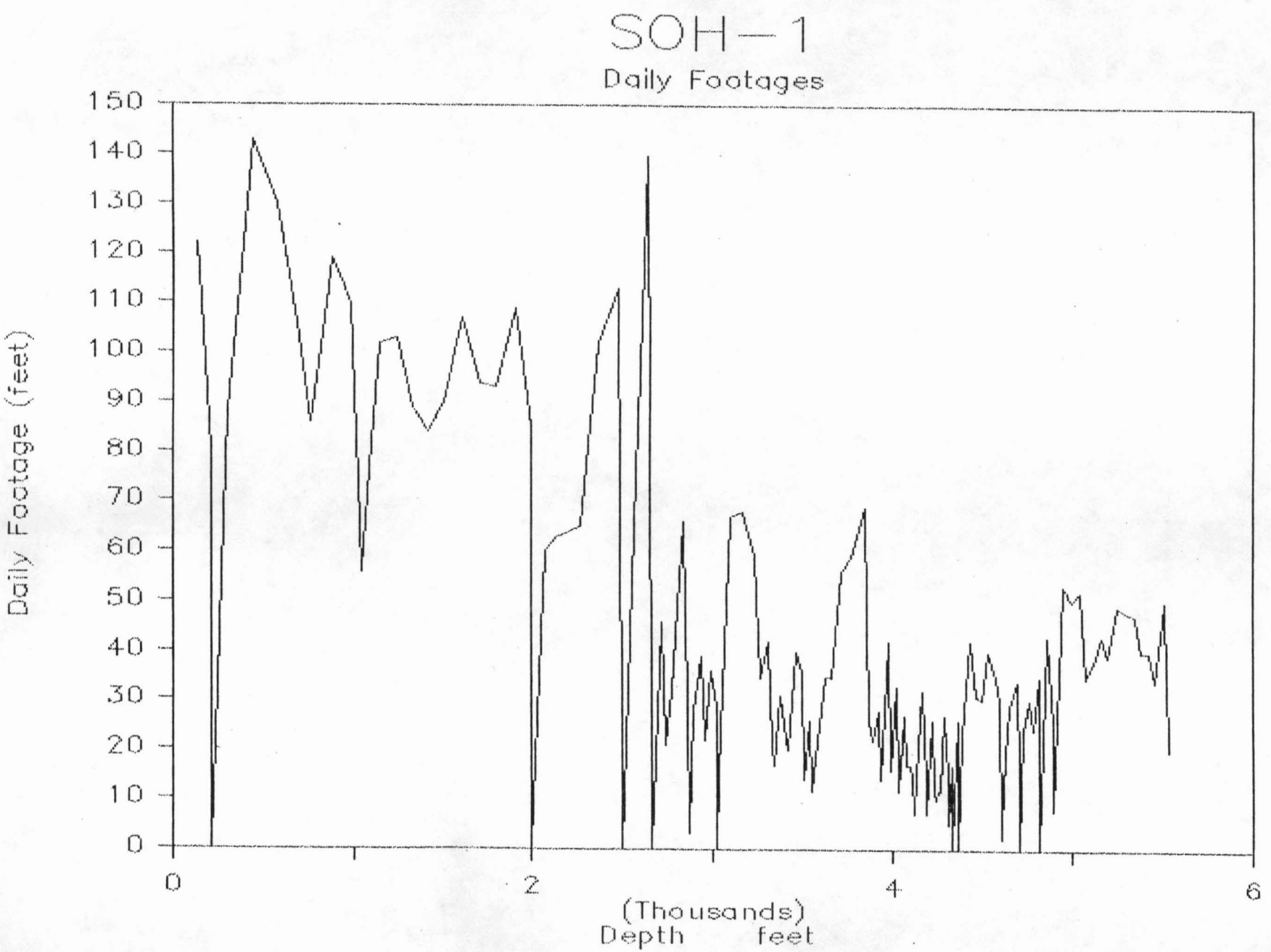

SOH-1
Drilling Costs/Foot
0
-1
-2
-3
-4
-5
-6
-7
Depth - feet
(Thousands)
0
200
400
600
800
Cost/Foot

Figure 6


SOH-1
Daily Footages
Daily Footage (feet)
150
140
130
120
110
100
90
80
70
60
50
40
30
20
10
0
0
2
4
6
(Thousands)
Depth feet

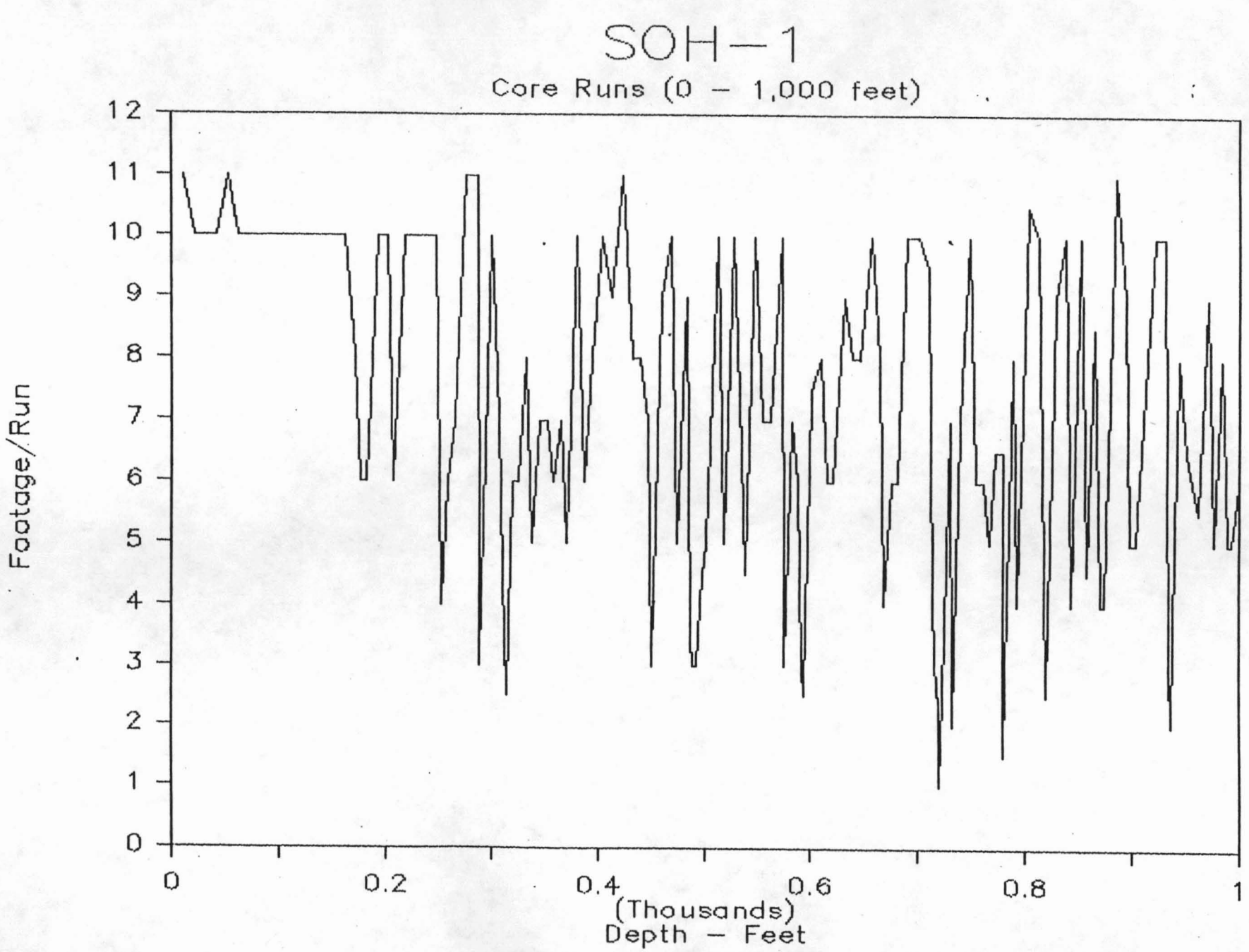

SOH-1
Core Runs (0 - 1,000 feet)
Footage/Run
12
11
10
9
8
7
6
5
4
3
2
1
0
0
0.2
0.4
0.6
0.8
1
(Thousands)
Depth - Feet

Figure 7a

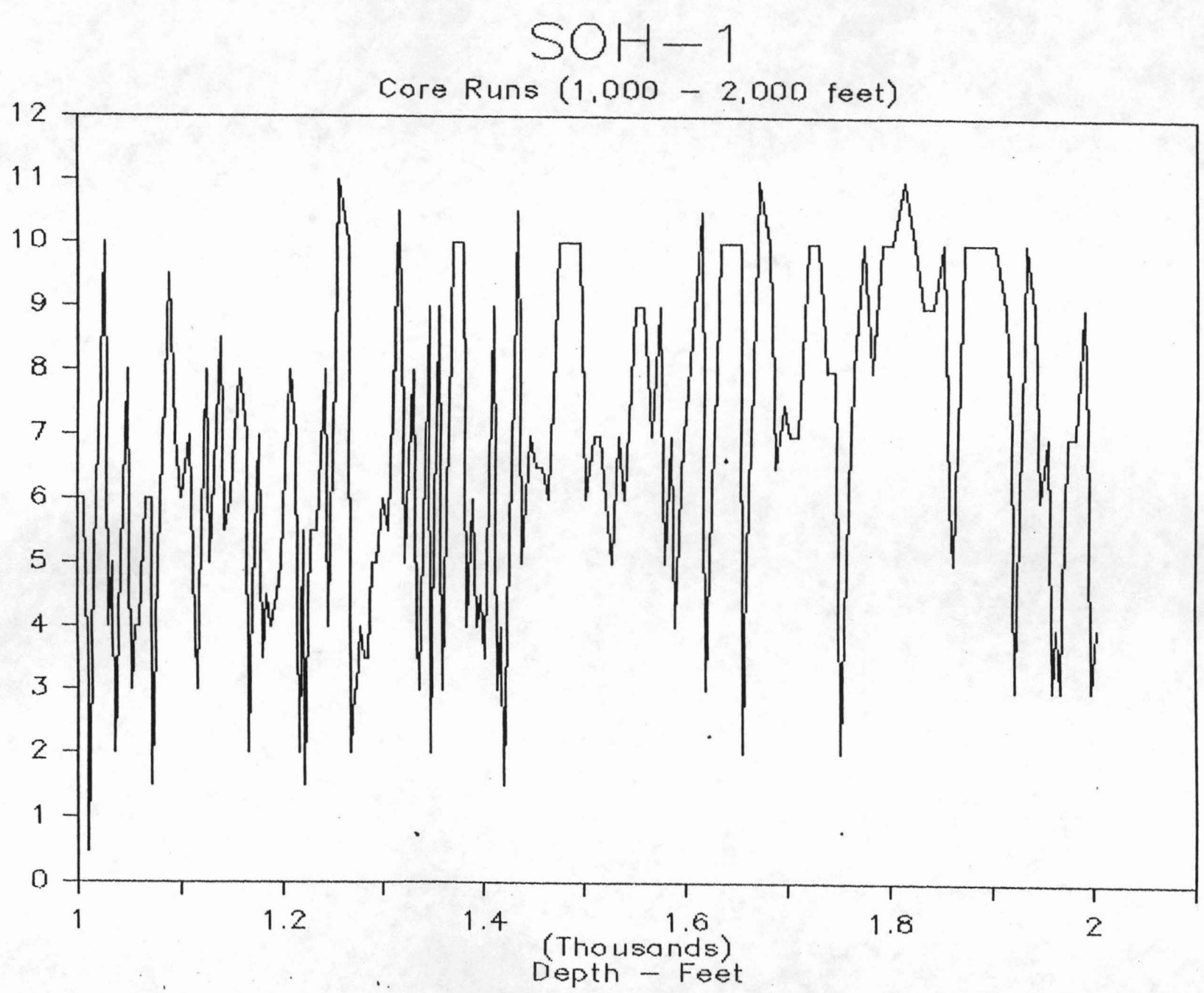

SOH-1
Core Runs (1,000 - 2,000 feet)
Footages/ Run
12
11
10
9
8
7
6
5
4
3
2
1
0
1
1.2
1.4
1.6
1.8
2
(Thousands)
Depth - Feet

Figure 7b

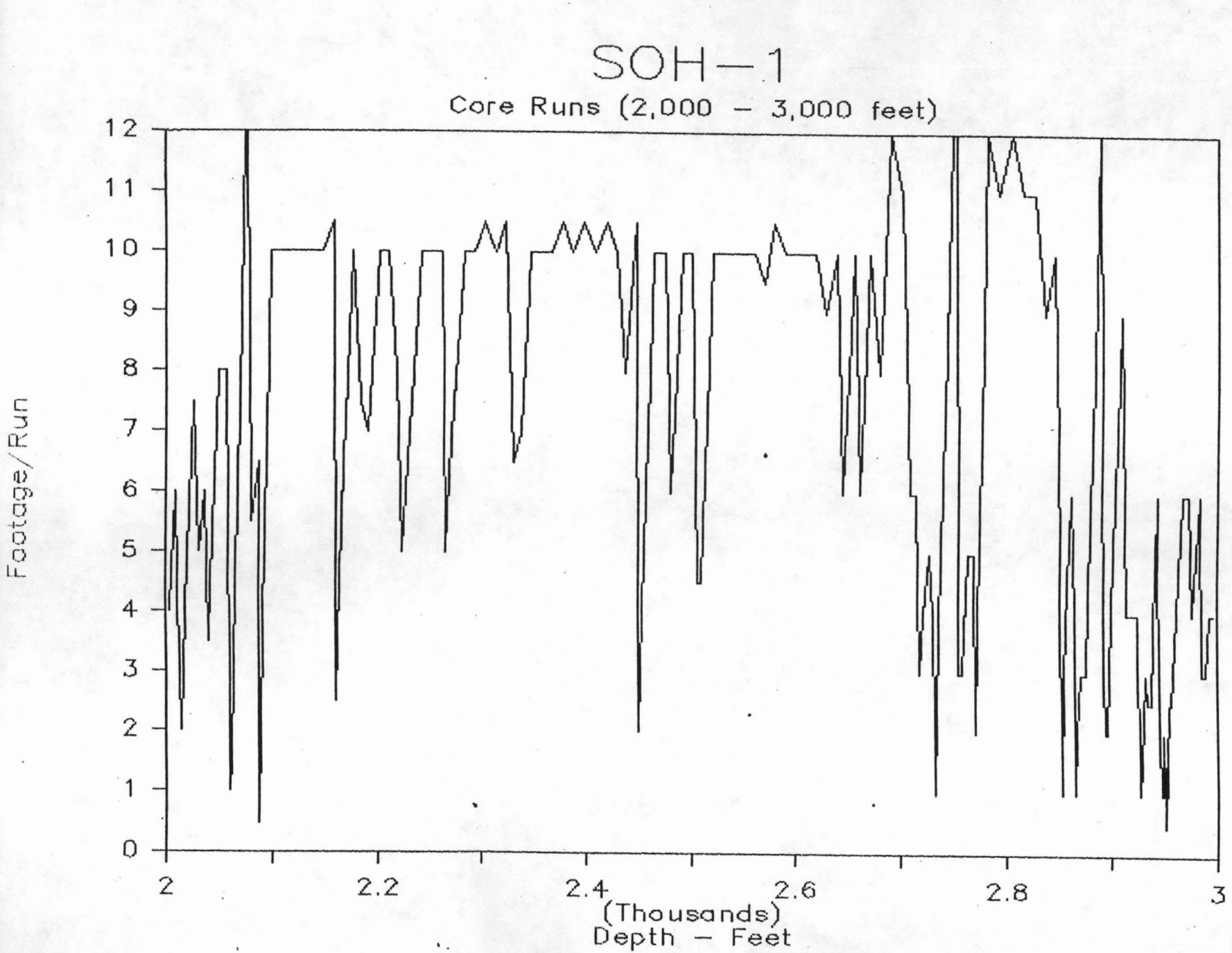

SOH—1
Core Runs (2,000 – 3,000 feet)
Footage/Run
12
11
10
9
8
7
6
5
4
3
2
1
0
2
2.2
2.4
2.6
2.8
3
(Thousands)
Depth – Feet

Figure 7c

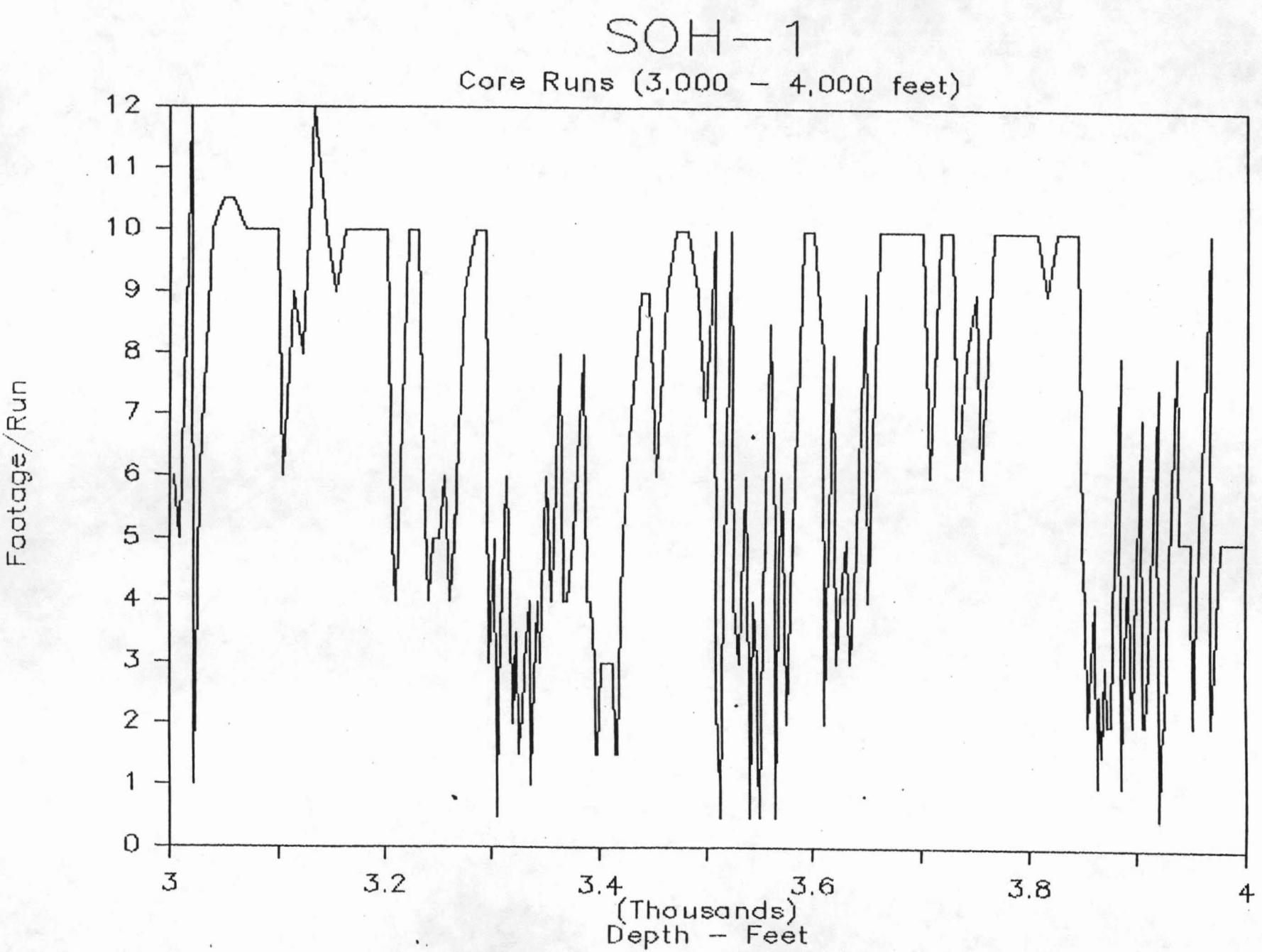

SOH-1
Core Runs (3,000 - 4,000 feet)
Footage/Run
12
11
10
9
8
7
6
5
4
3
2
1
0
3
3.2
3.4
3.6
3.8
4
(Thousands)
Depth - Feet

Figure 7d

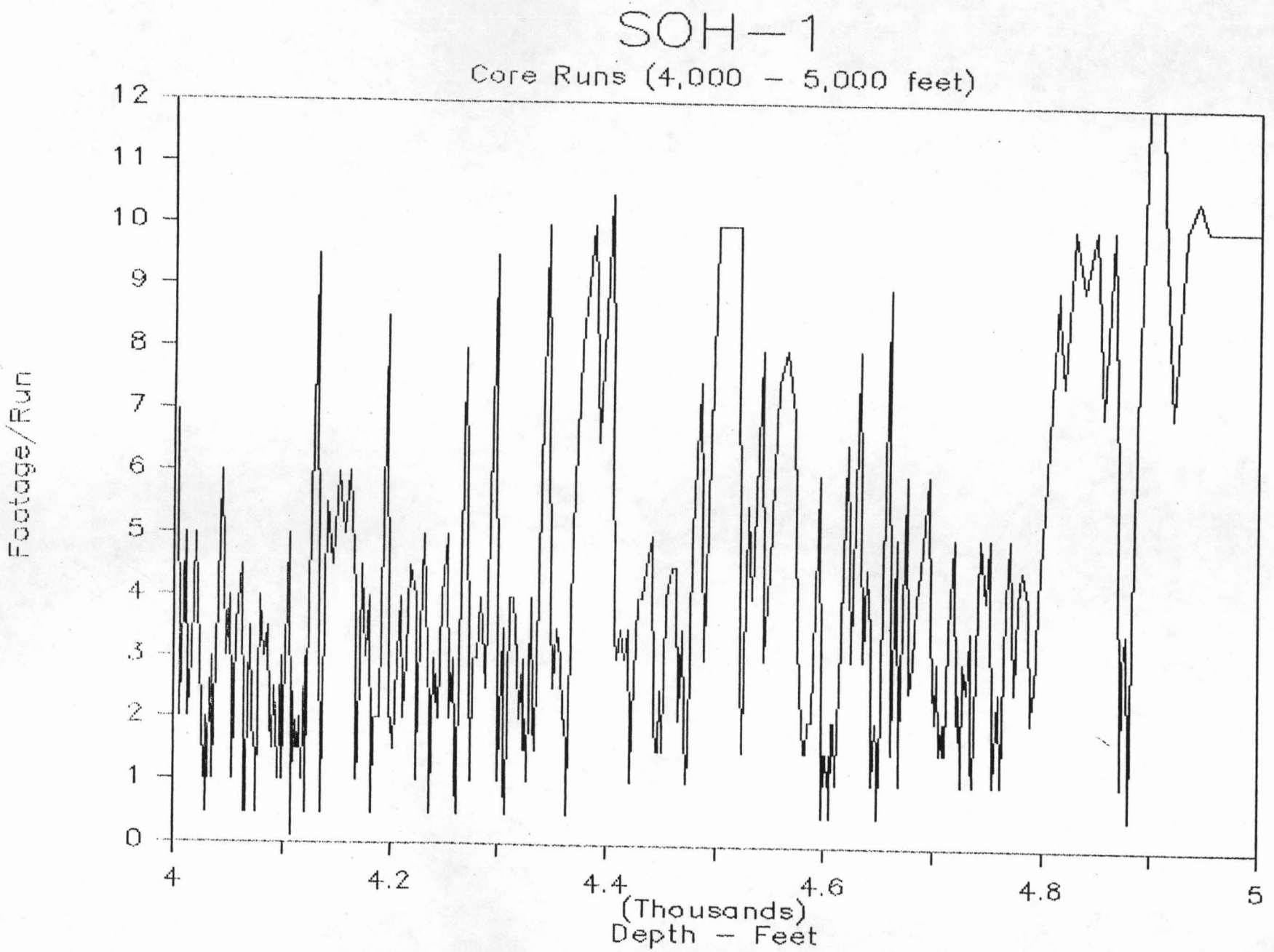

SOH-1
Core Runs (4,000 - 5,000 feet)
Footage/Run
12
11
10
9
8
7
6
5
4
3
2
1
0
4
4.2
4.4
4.6
4.8
5
(Thousands)
Depth - Feet

Figure 7e

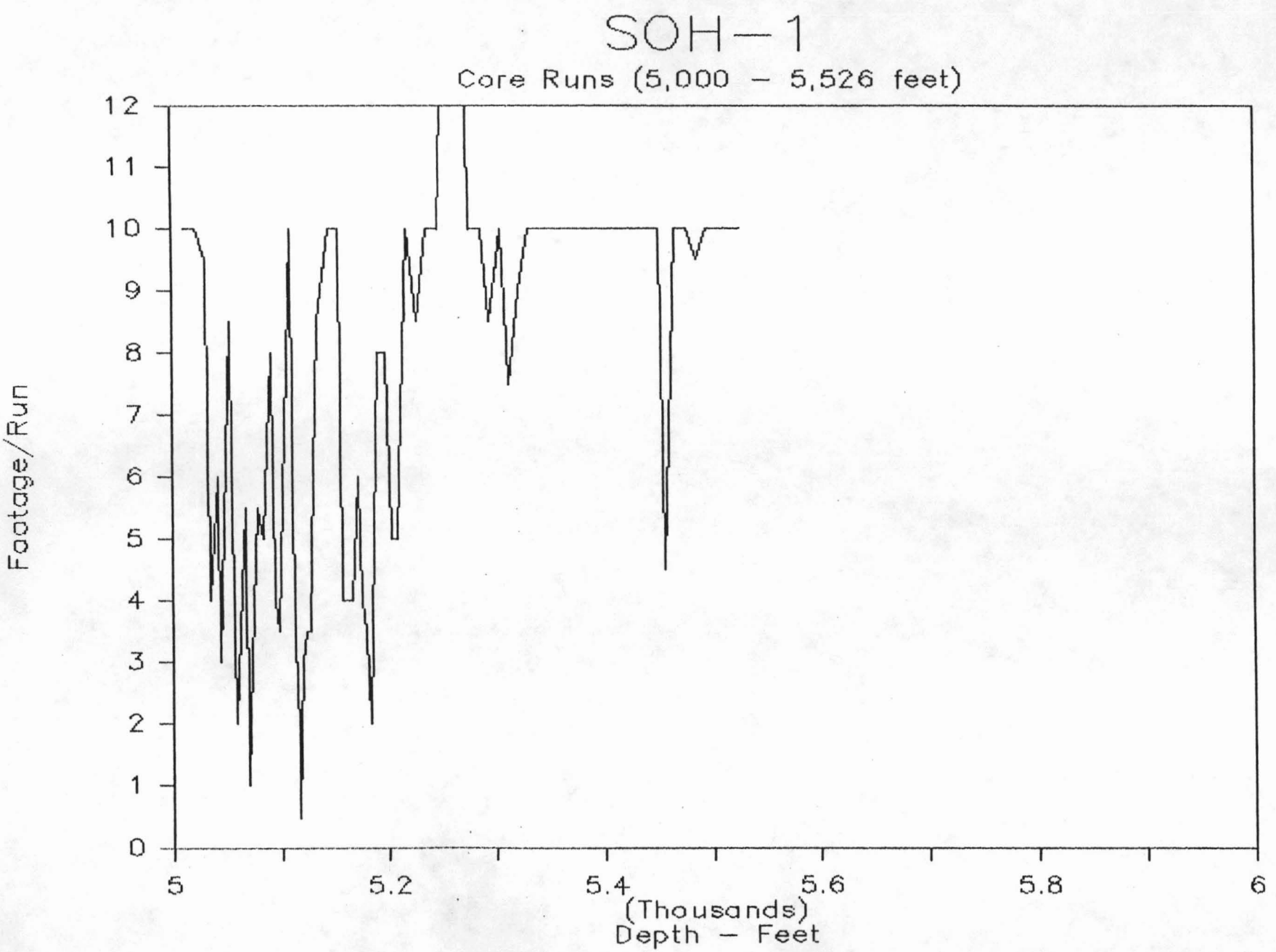
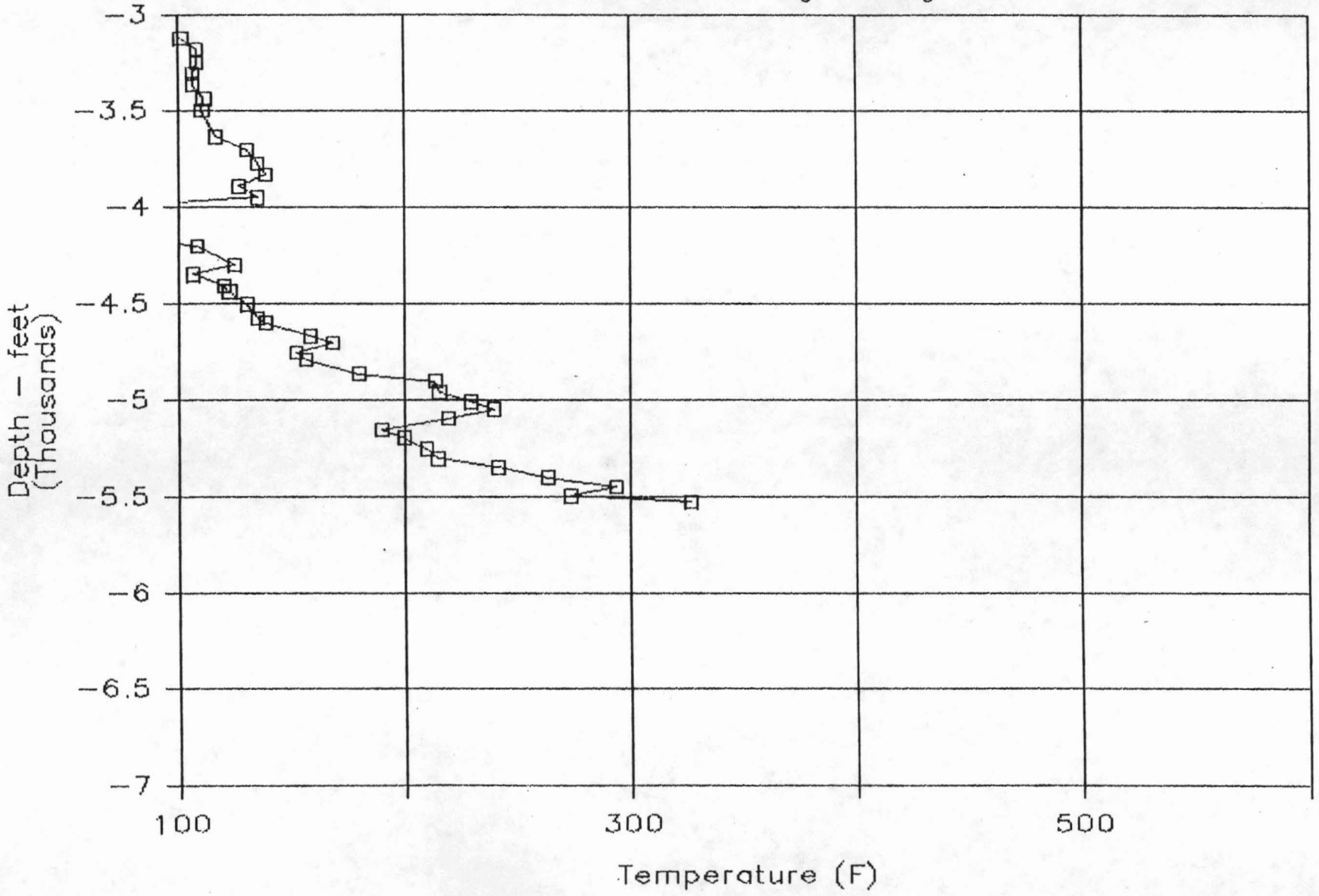

SOH-1
Core Runs (5,000 - 5,526 feet)
Footage/Run
12
11
10
9
8
7
6
5
4
3
2
1
0
5
5.2
5.4
5.6
5.8
6
(Thousands)
Depth - Feet

Figure 7f

Figure 8

# SOH-1 BOTTOM HOLE TEMPERATURES

Measured During Drilling



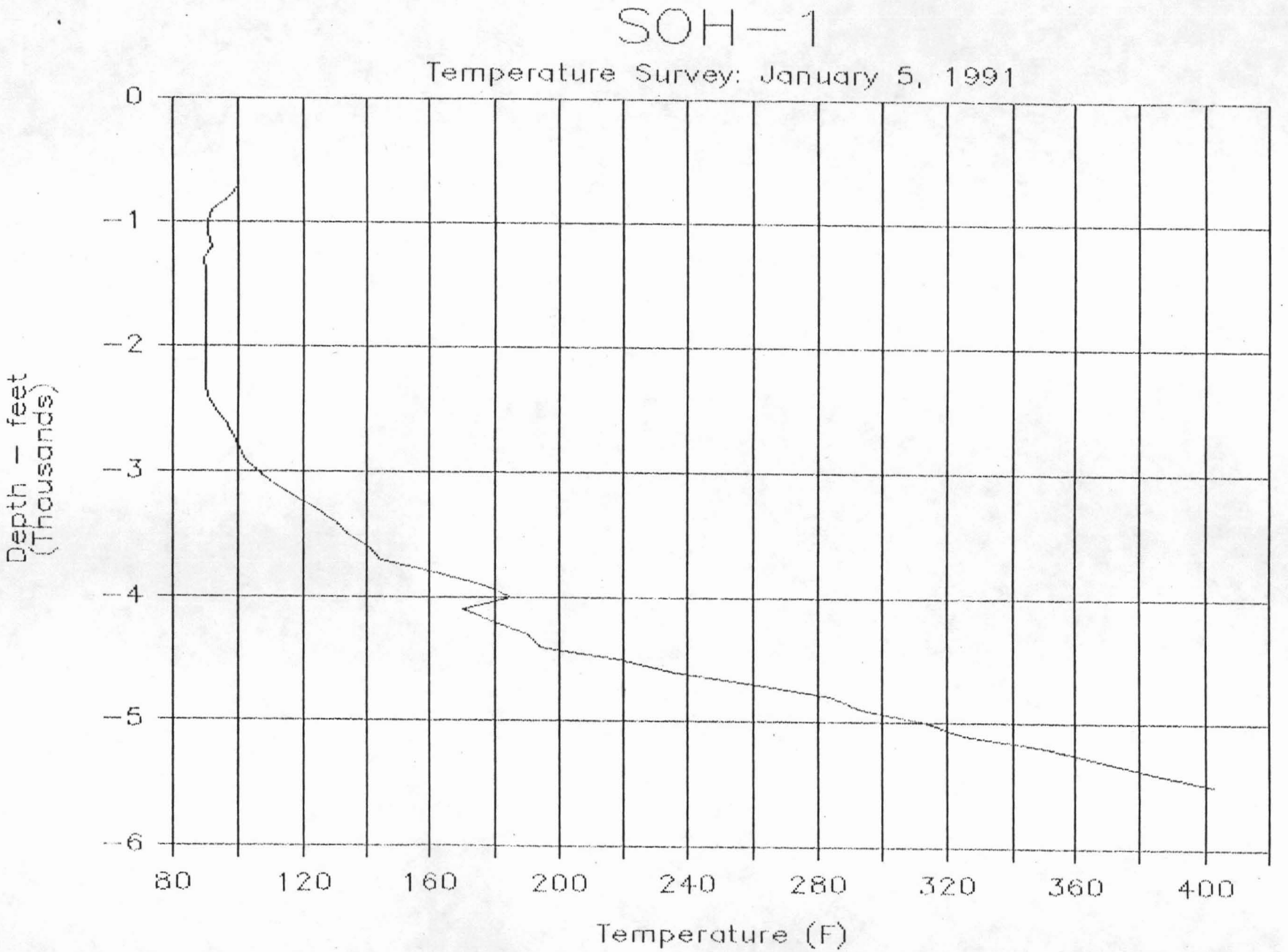

SOH-1
Temperature Survey: January 5, 1991
Depth - feet (Thousands)
0
-1
-2
-3
-4
-5
-6
80
120
160
200
240
280
320
360
400
Temperature (F)

Figure 9

Figure 10

Completed SOH-1 Schematic

0 - 202 ft. - 12-1/4" hole
9-5/8" K-55, 40#/ft. casing
Cemented w/ redimix concrete

202 - 1,996 ft. - 8-1/2" hole
7" L-80, K-55, 35#/ft. casing
Cemented w/ silica/spherelite cement

1,996 - 2,671 ft. - 5-7/8" hole

2,671 - 3,022 ft. - CHD-134 hole (5.27")
4-1/2" casing 0-3,022 ft.
0-2,005 ft. J-55, 10.5 #/ft., ST&C
2,005 - 3,022 ft. J-55, 11.6#/ft., flush joint
Bottom 200 ft. cemented w/ neat cement

3,022 - 4,325 ft. - HQWL hole (3.83" hole x 2.50" core)

4,325 - 5,526 ft. - NQ hole (2.98" hole x 1.875" core)

Completion tubing - NQ (2.75" O.D. x 2.375" I.D.)
5.2#/ft., perforated w/ 1/2" holes on 6" centers

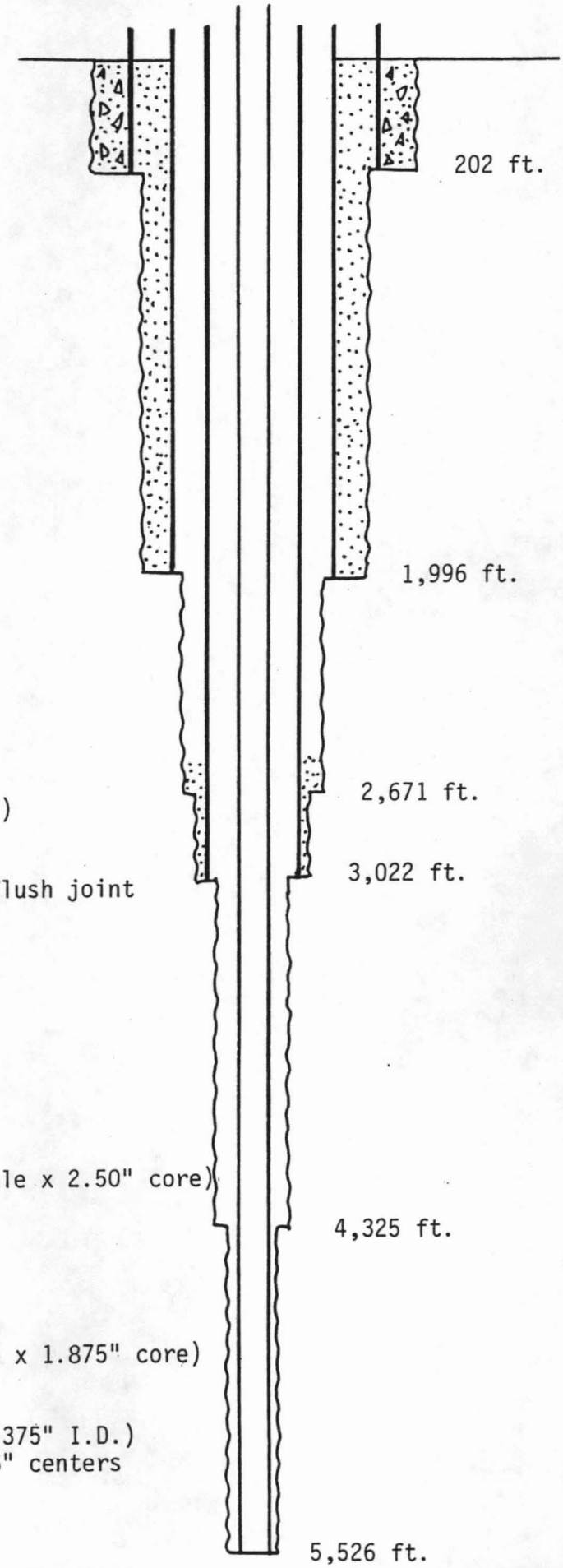


Figure 11

SOH-1 Completion Wellhead

1. Companion Flange - 2-9/16" 3M x 3" L.P.
2. Gate Valve - 2-9/16" Foster Flow-Seal w/ T-24 trim
3. Tubing Head Adapter - 7-1/16" 3M x 2-9/16" 3M
4. 7" EFSO Slip On Wellhead
5. Gate Valves - 2-1/16" 3M Foster Flow-Seal w/ T-24 trim
6. Companion Flanges - 2-1/16" 3M x 2" L.P.
7. 7" L-80, 35#/ft. casing
8. NQ Completion Tubing (2.75" O.D., 5.5#/ft.)
9. 9-5/8" K-55, 40#/ft. casing